

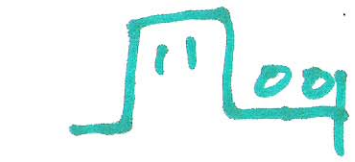
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Lecture 26

02.00

ELG 722

Mixed-signal



7.5



$$V_{out}(z) = \frac{z^{-1}}{1 + \frac{C_I}{C_F} \cdot \frac{1}{A_{OL}}} \cdot V_{in} + V_{OP}(\quad)$$

EQ.7.32

$$\Sigma = \frac{C_I}{C_F} \cdot \frac{1}{A_{OL}} \quad \text{EQ 7.33}$$

$$\left| \frac{V_{in} z^{-1}}{1 + \Sigma} \right|$$

$$\frac{V_{in}}{1.1} \approx 0.9 V_{in}$$

$$A_{OL} = 10, \quad \frac{C_I}{C_F} = 1$$

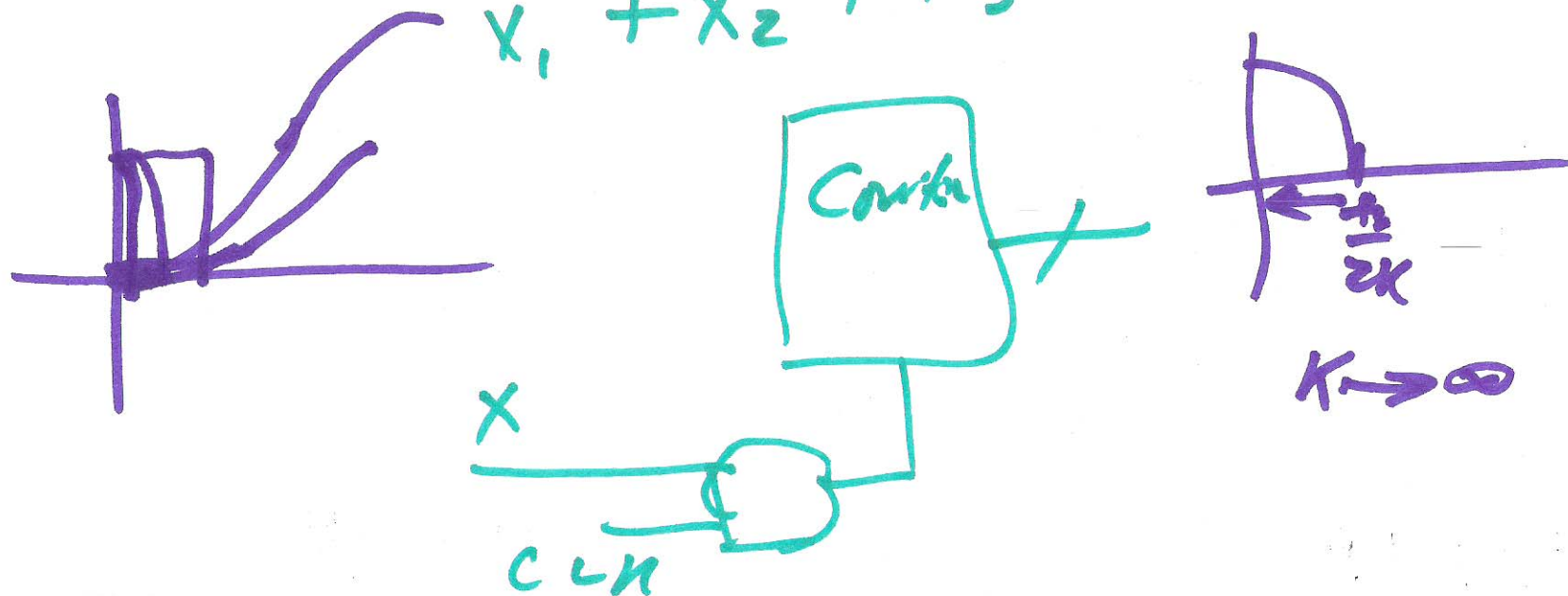
finite sense functional) start-up

$$\sum_{k=1}^{\infty} \{x_1 + x_2 + \dots + x_k\} = (1 + z^{-1} + z^{-2})X = Y$$

$$H = \frac{Y}{X} = \frac{1 - z^{-k}}{1 - z^{-1}}$$

Counter

$$x_1 + x_2 + x_3 + \dots + x_k$$



$$\frac{v_1(z) \cdot z^{-1/2} - v_2(z)}{1 + z^{-1}} \quad \frac{C_I}{C_F} = 202T$$

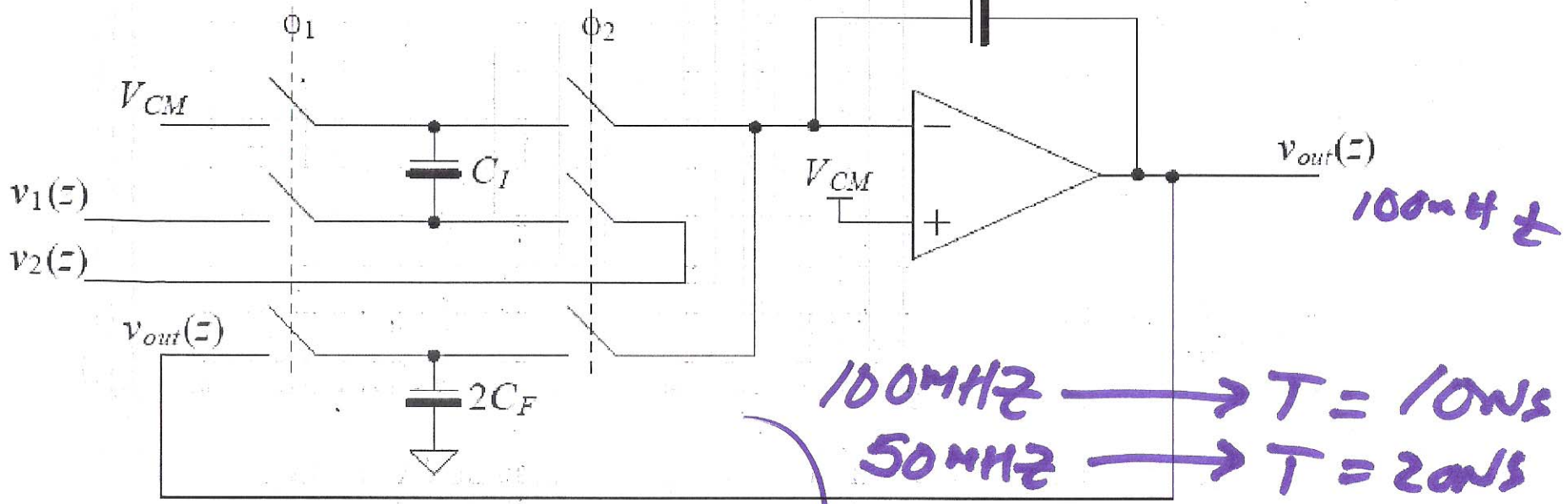
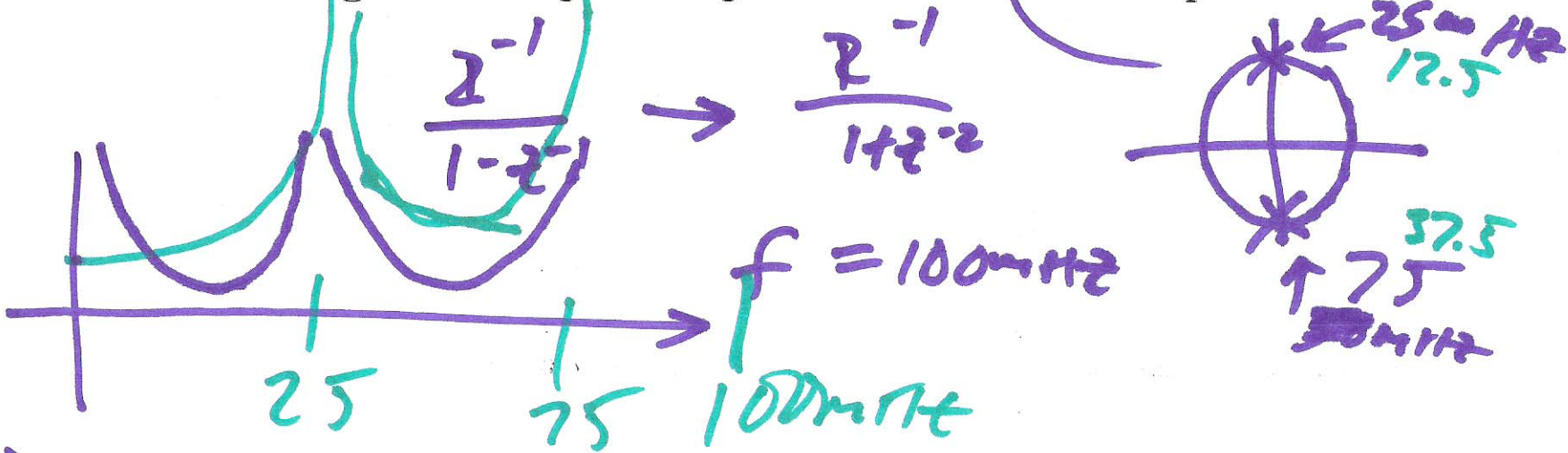
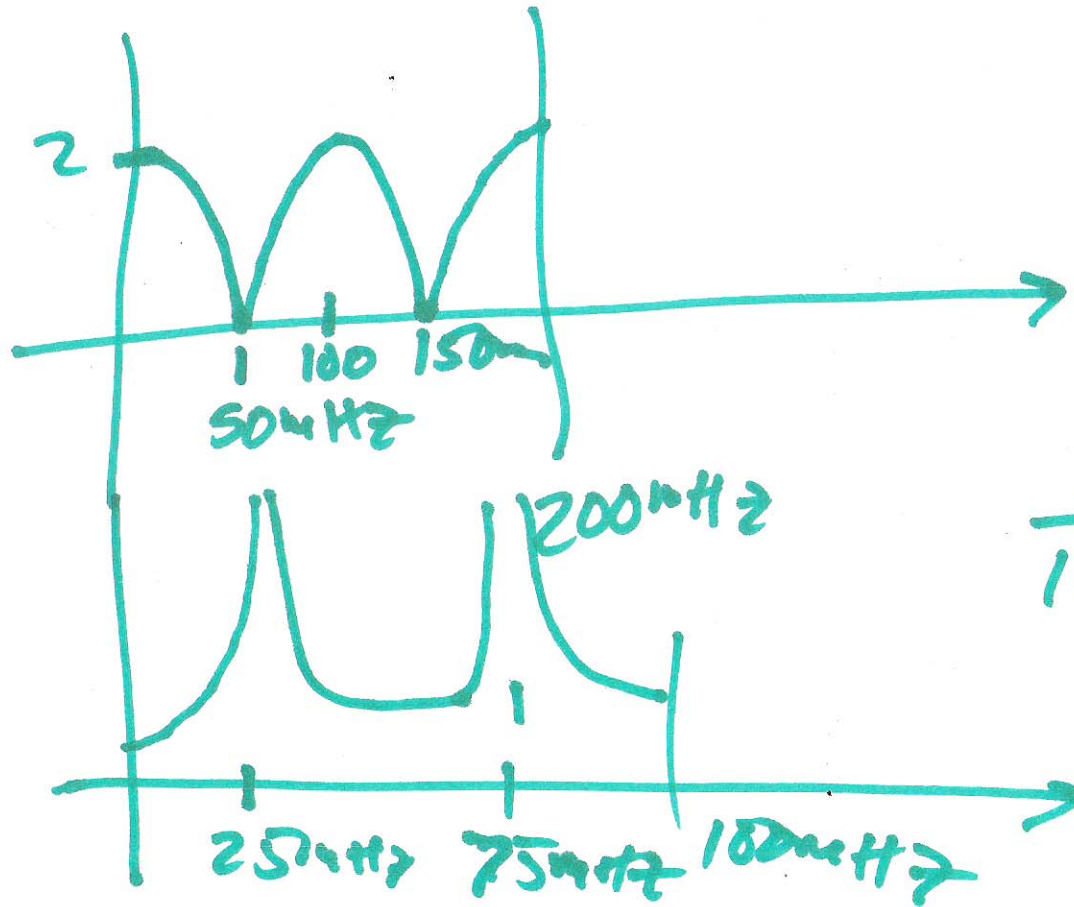


Figure 8.12 Implementing a resonator for use in a bandpass modulator.



3)

$$1 + z^{-1} \quad f_s = 100 \text{ kHz}$$



$$\frac{1}{1+z^{-2}} = \frac{z^2}{z^2+1}$$

$f_s = 50 \text{ kHz}$

$A = 100 \text{ kHz}$

4)

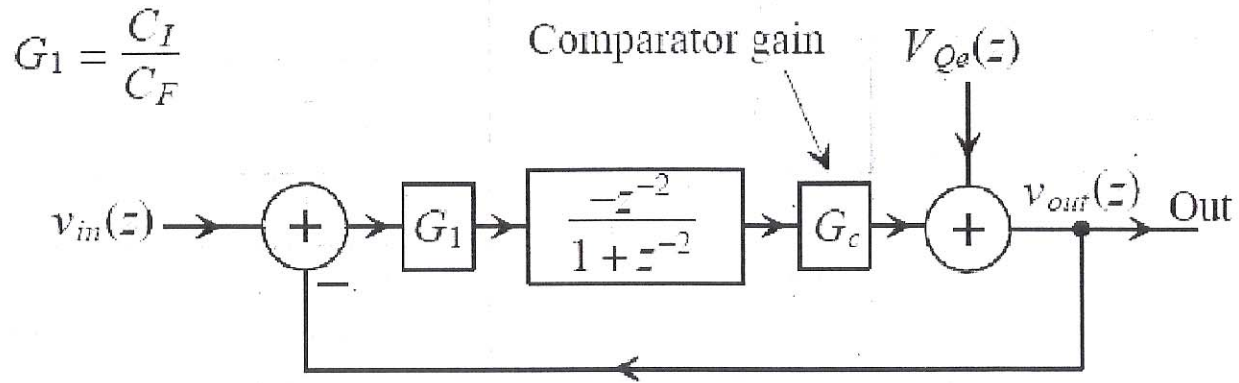


Figure 8.13 Block diagram of a second-order bandpass modulator.



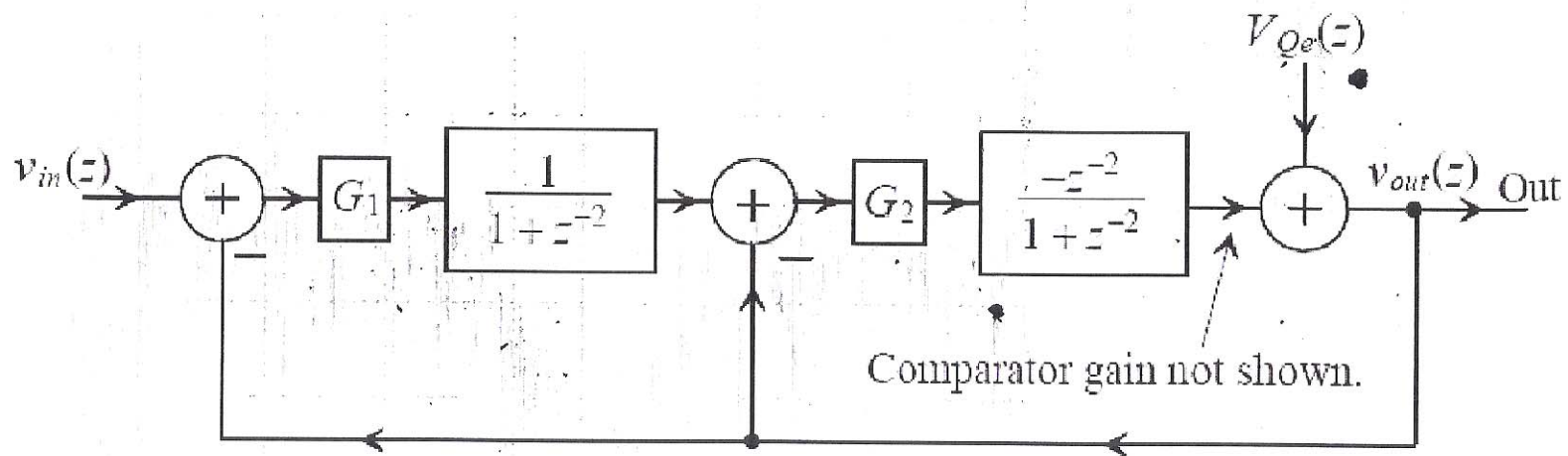


Figure 8.15 A fourth-order bandpass modulator.

$$\left(\frac{(v_{in} - v_{out})G_1}{1 + z^{-2}} - v_{out} \right) G_2 \left(\frac{-z^{-2}}{1 + z^{-2}} \right) + V_{Qe} = v_{out}$$

$$\left((v_{in} - v_{out})G_1 - v_{out}(1 + z^{-2}) \right) G_2 \cdot (-z^{-2}) + V_{Qe}(1 + z^{-2}) = v_{out}(1 + z^{-2})^2$$

b)

$$V_{in} G_1 G_2 (-z^{-2}) + V_{nT} G_1 G_2 z^{-2} + V_{nT} G_2 (1+z^{-2}) z^{-2} + V_{dP} (1+z^{-2})^2 = V_{nT} (1+z^{-2})^2$$

$$-V_{in} \cdot G_1 G_2 z^{-2} + V_{dP} (1+z^{-2})^2 = V_{nT} \left((1+z^{-2})^2 - G_1 G_2 z^{-2} \right)$$

$$\cancel{1 + 2z^{-2} + z^{-4}} - \cancel{z^{-2} - z^{-2} - z^{-4}} - G_2 (1+z^{-2}) z^{-2}$$

$$V_{nT} = -V_{in} z^{-2} + V_{dP} (1+z^{-2})^2$$

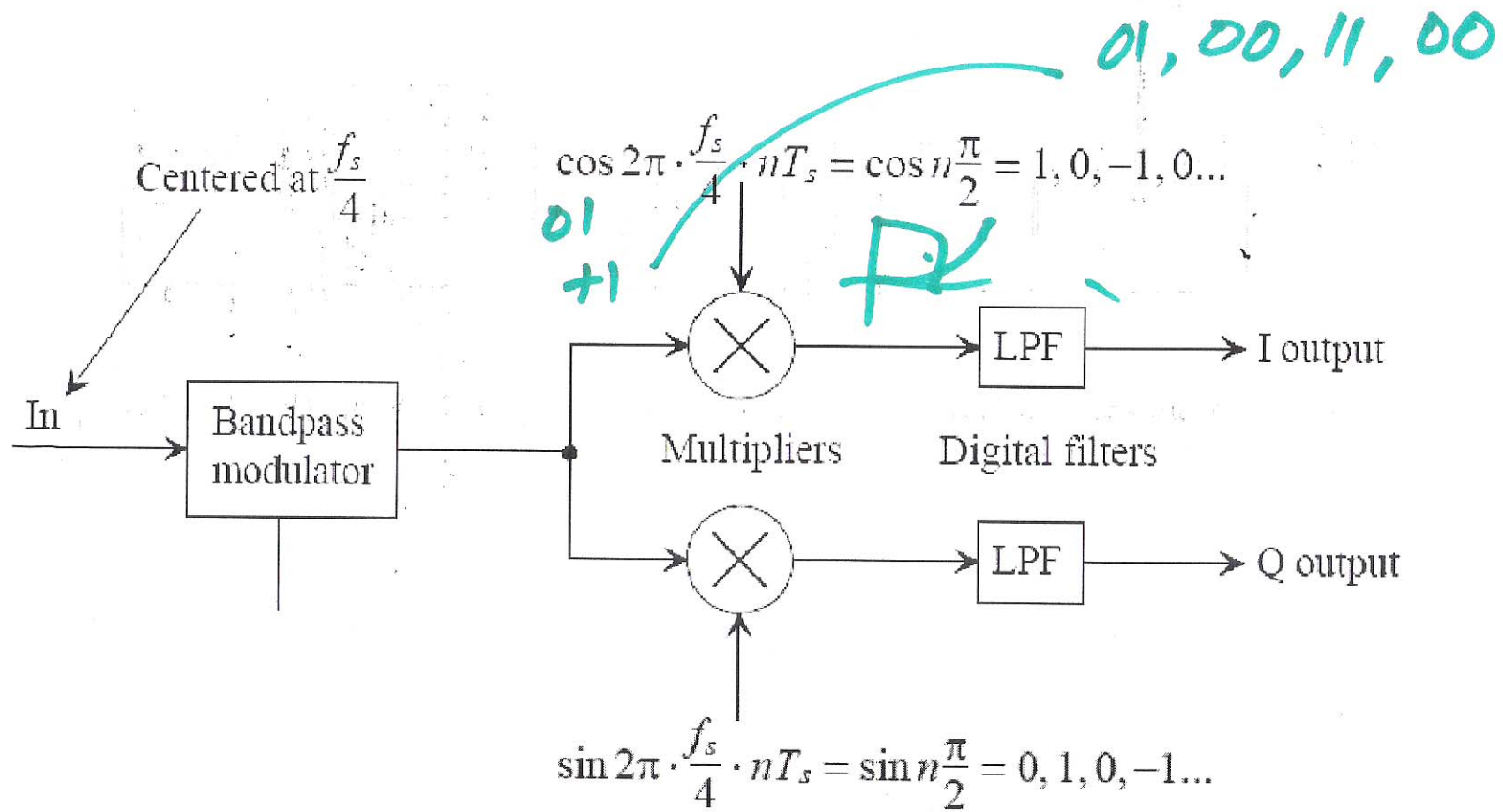


Figure 8.18 Digital I/Q demodulation.