

# 7.2 Second-order Noise-Shaping

first-order

$$V_{out}(z) = V_{in}(z) \cdot z^{-1} + V_{qd}(z) \cdot (1 - z^{-1})$$

second-order

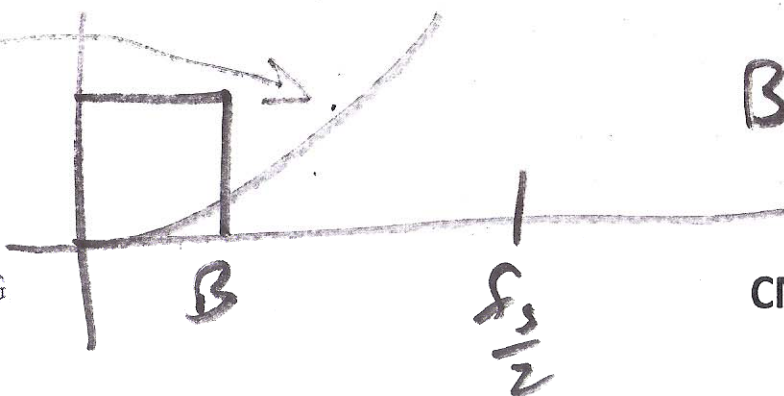
$$V_{out}(z) = V_{in}(z) \cdot z^{-1} + V_{qd}(z) (1 - z^{-1})^2$$

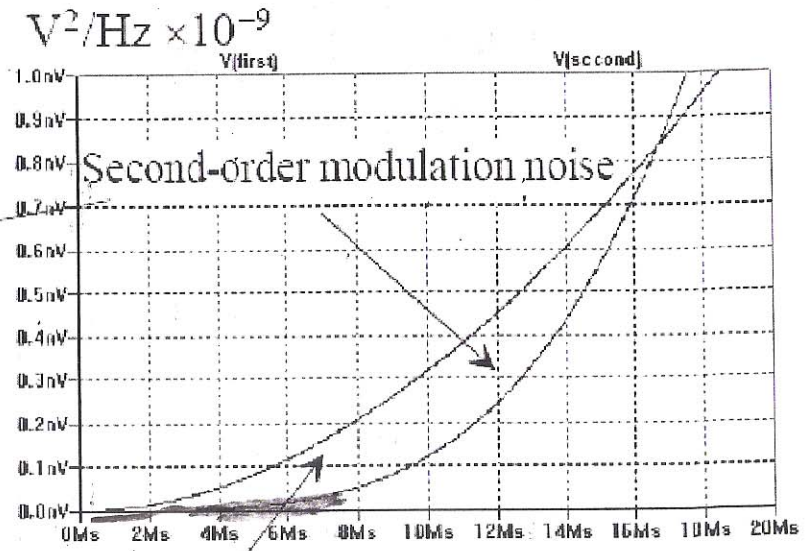
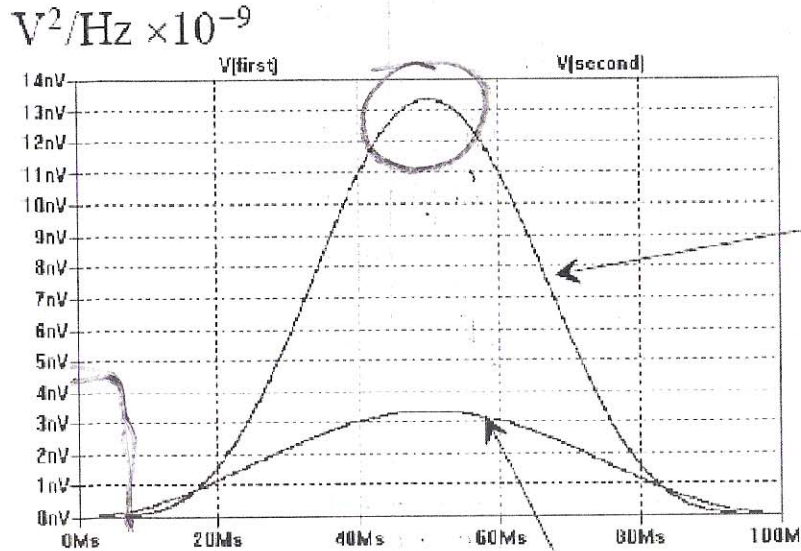
$$\int_0^B |NTF(f)|^2 \cdot |V_{qd}(f)|^2 df = \frac{V_{LSB}^2}{12 f_s} \cdot 16 \sin^4 \left( \pi \frac{f}{f_s} \right) df$$

Modulation

$$V_{OE, rms} \approx \frac{V_{LSB}}{\sqrt{12}} \cdot \frac{\pi^2}{\sqrt{5}} \cdot \frac{1}{k^{5/2}}$$

$$B = \frac{f_s}{2k}$$





First-order modulation noise

Figure 7.23 Comparing first- and second-order NS modulator's modulation noise.

$SNR_{ideal} = 6.02N + 1.76 - 12.9 + 50 \log k$   
 for every doubling in  $k$  you  
 get 15 dB improvement in SNR  
 $N \rightarrow 2.5 \text{ bits}$

2)

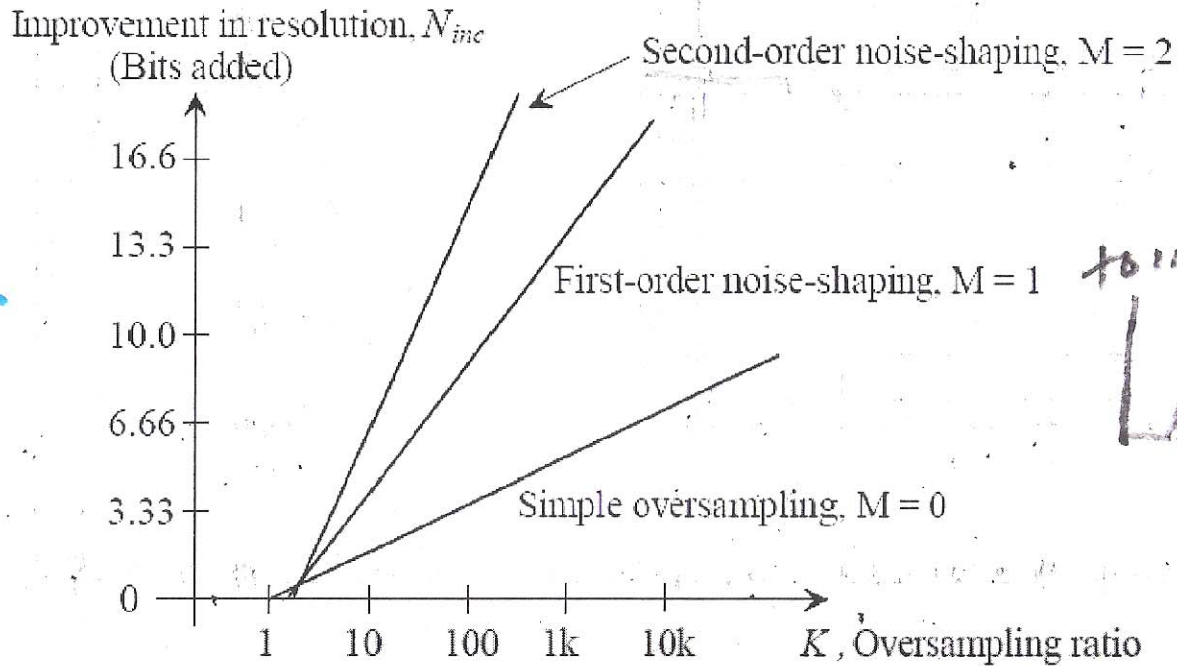
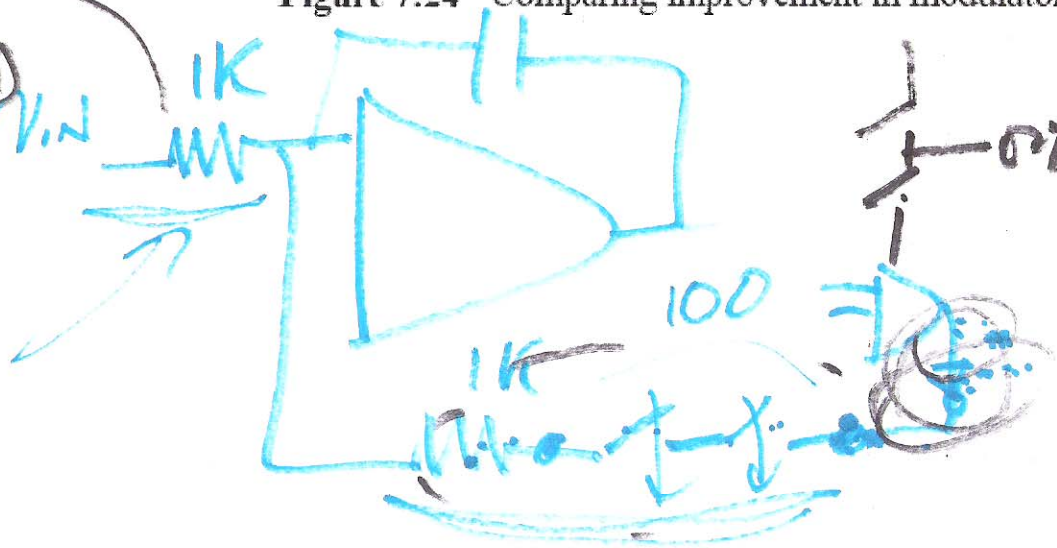
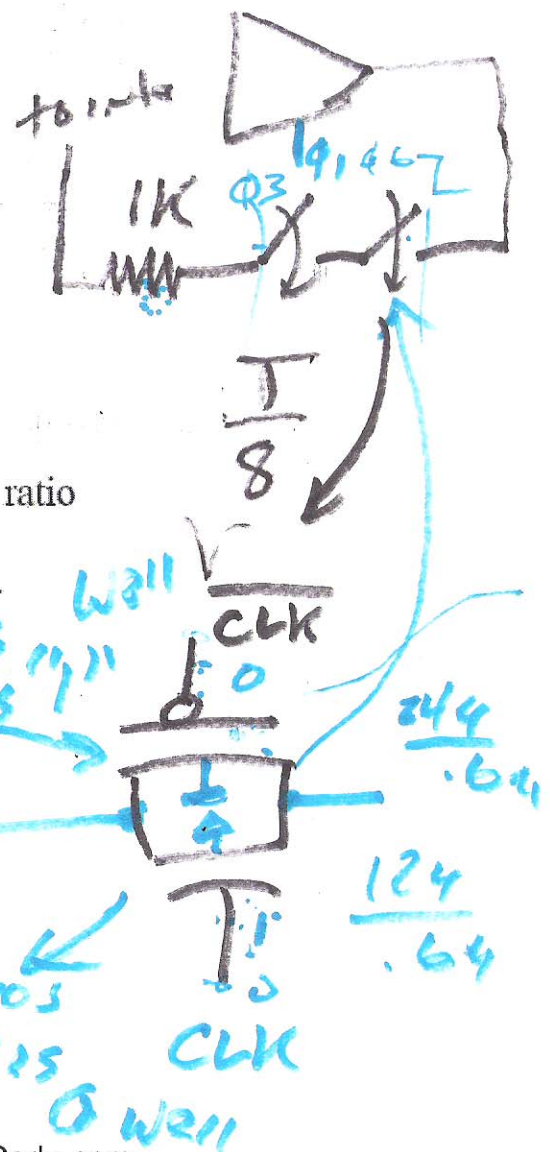


Figure 7.24 Comparing improvement in modulator resolution.



3)



$$V_{out}(z) = \frac{A(z)}{1 + A(z) \cdot B(z)} \cdot V_{in}(z) + V_{Qe}(z) \cdot \frac{1}{1 + A(z)B(z)}$$

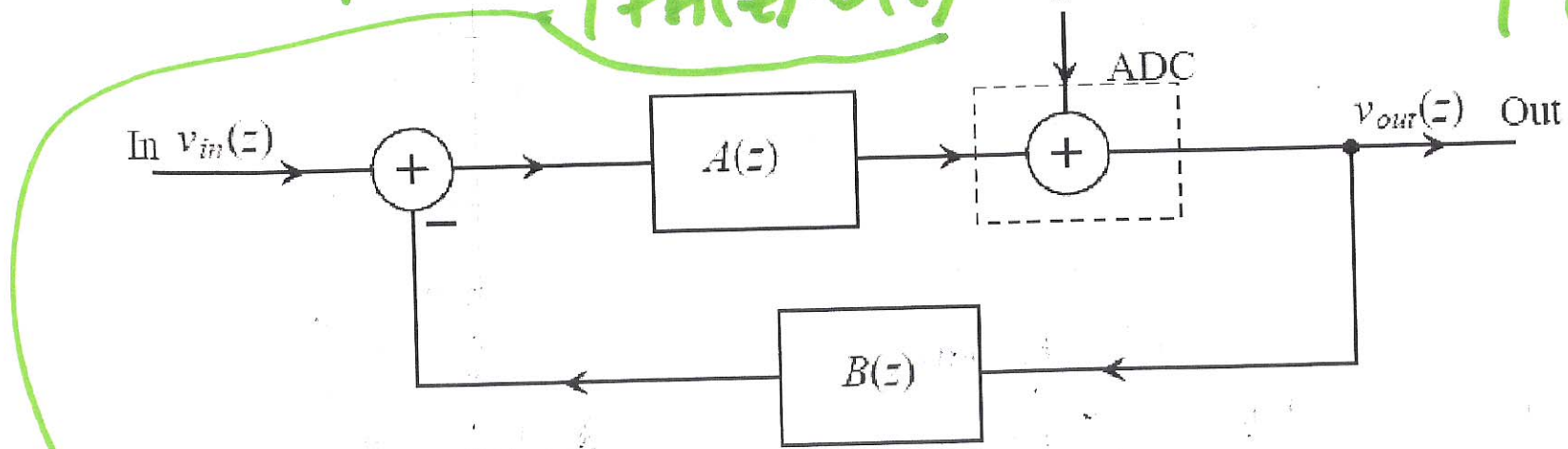


Figure 7.25 Block diagram of a feedback modulator.

$$\tilde{z}^{-1} = \frac{A(z)}{1 + A(z) \cdot B(z)}$$

$$(1 - \tilde{z}^{-1})^2 = \frac{1}{1 + A(z)B(z)}$$

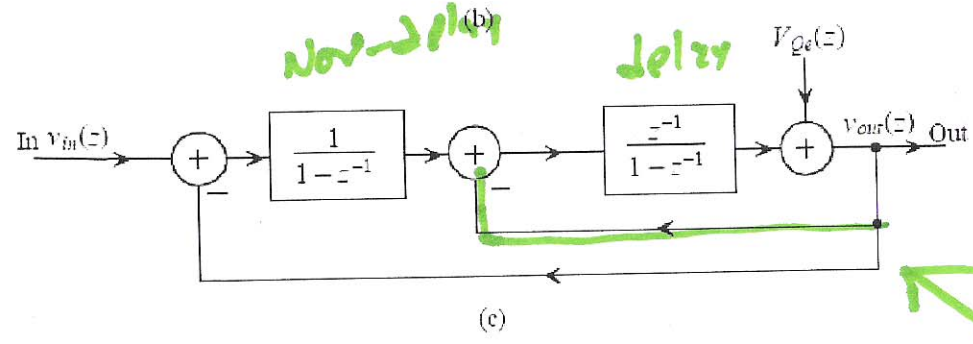
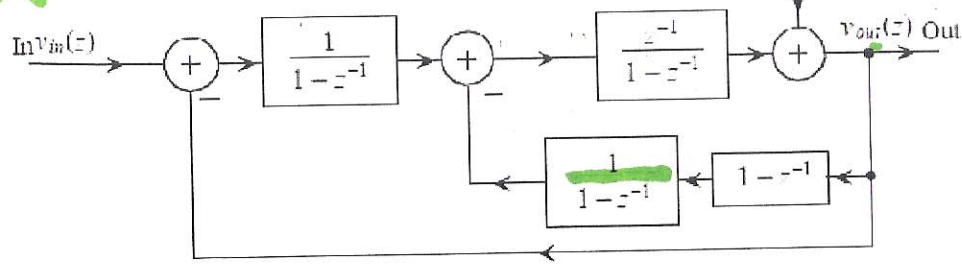
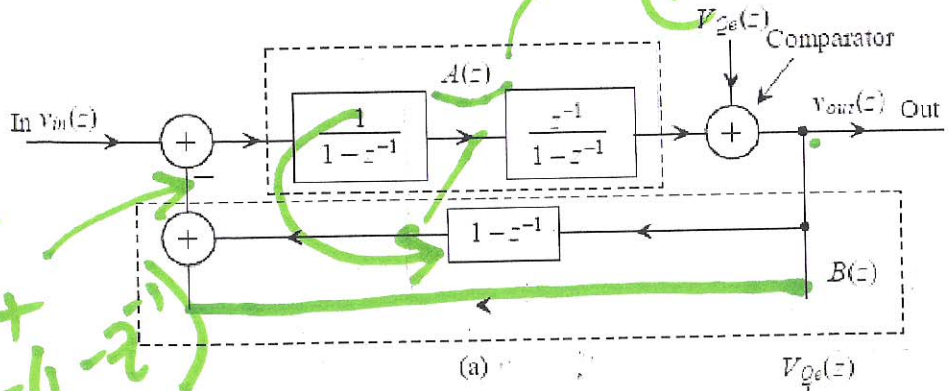
$$\frac{z^{-1}}{(1-z^{-1})^2} = A(z)$$

$$B(z) = 2 - z^{-1}$$

$$V_f = V_{OUT} (2 - z^{-1})$$

$$B(z) = \frac{V_f}{V_{OUT}} = 2 - z^{-1}$$

$V_f$   
 $V_{OUT} +$   
 $V_{OUT}(1 - z^{-1})$



topology for  
 2nd-order  
 noise-shaping.

Figure 7.26 Block diagrams of second-order modulators.

5)

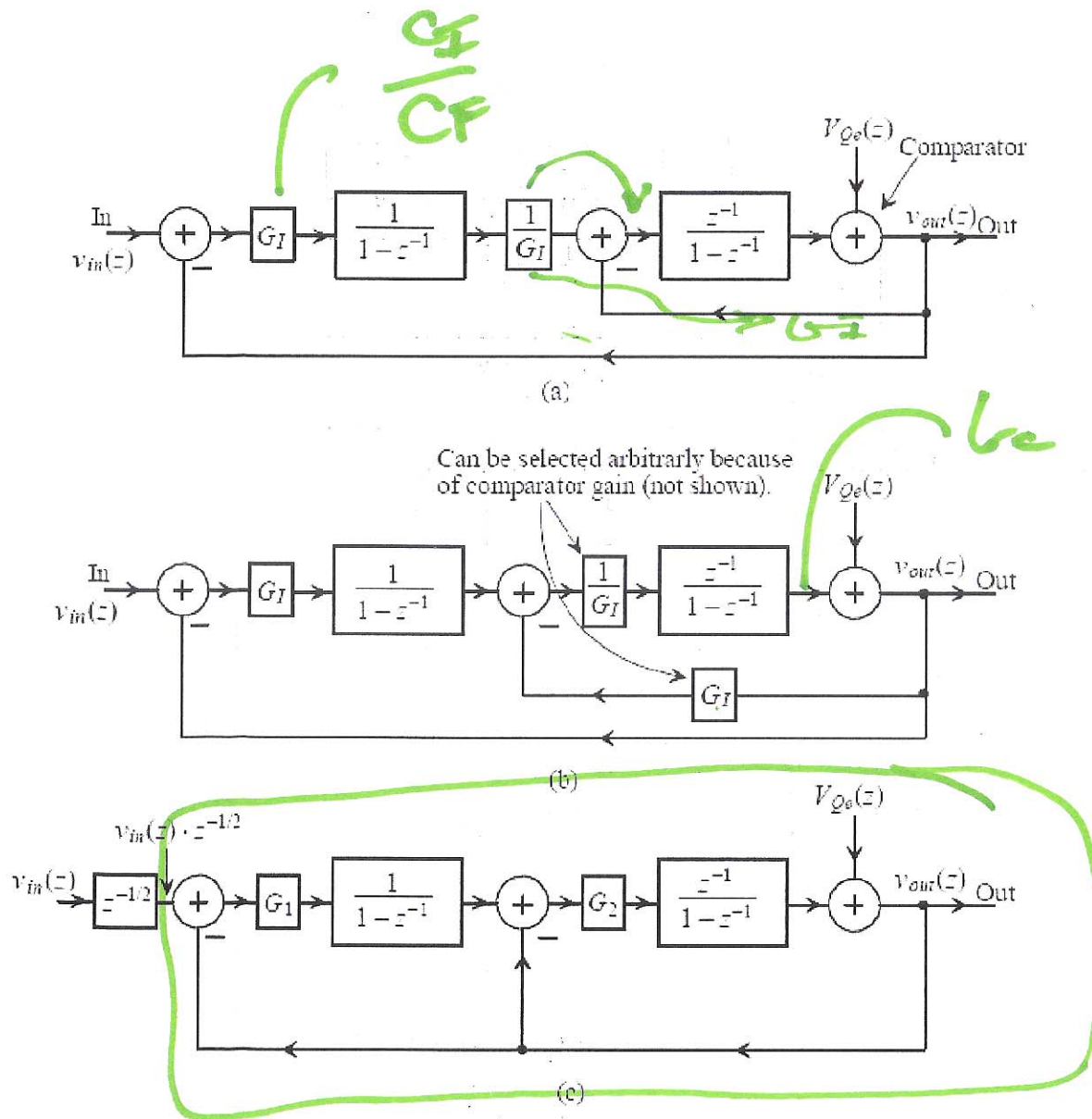


Figure 7.27 Block diagrams of second-order modulator introducing integrator gains.

6)

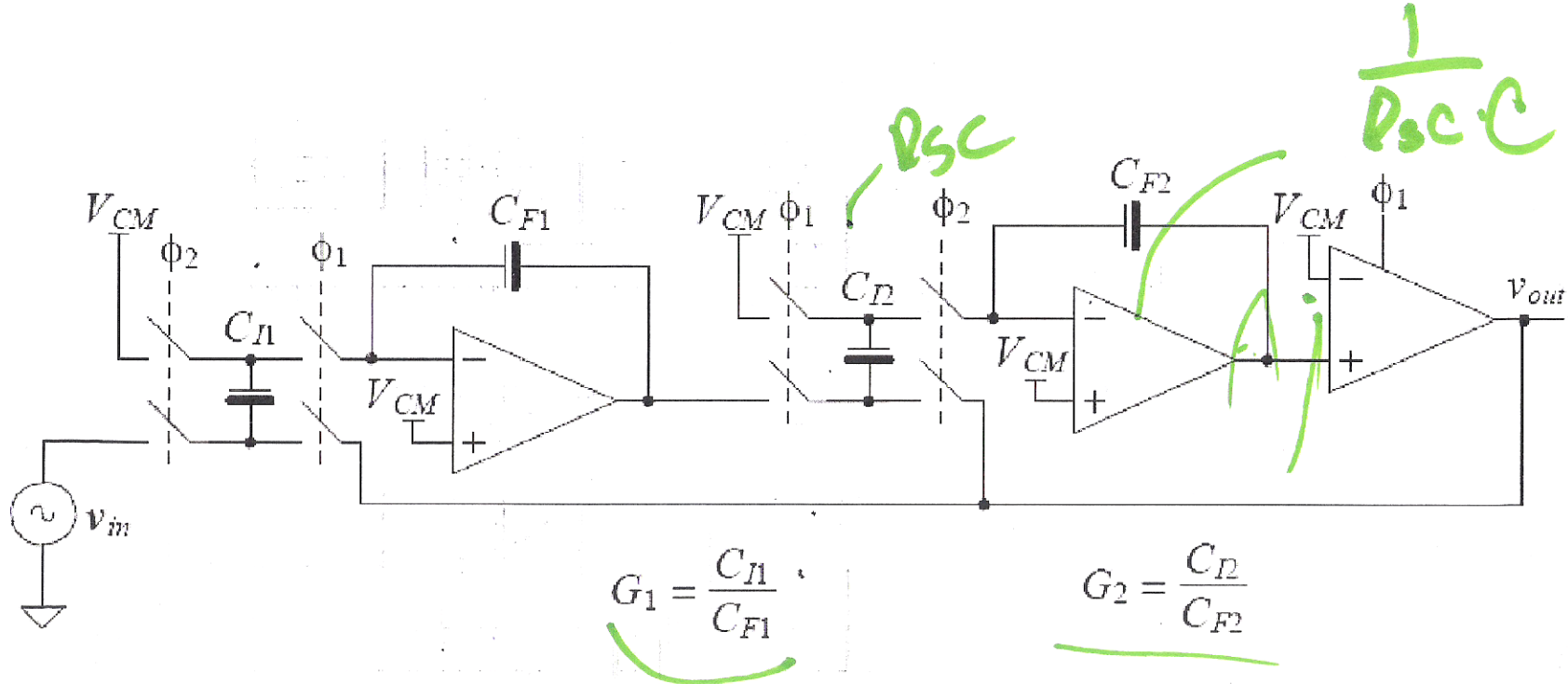
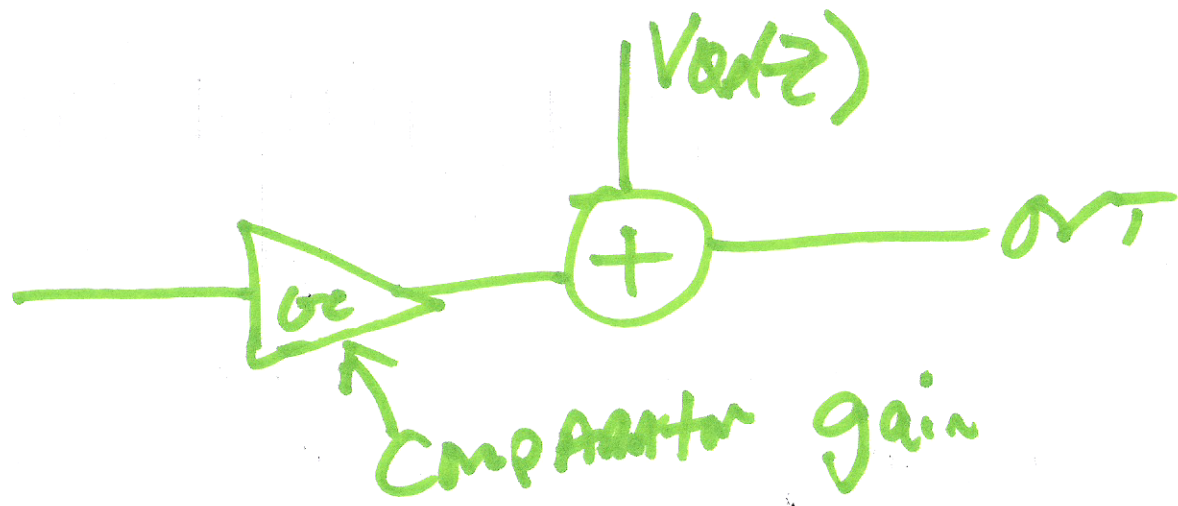


Figure 7.28 Implementation of the second-order modulator of Fig. 7.27c.



Comparator gain



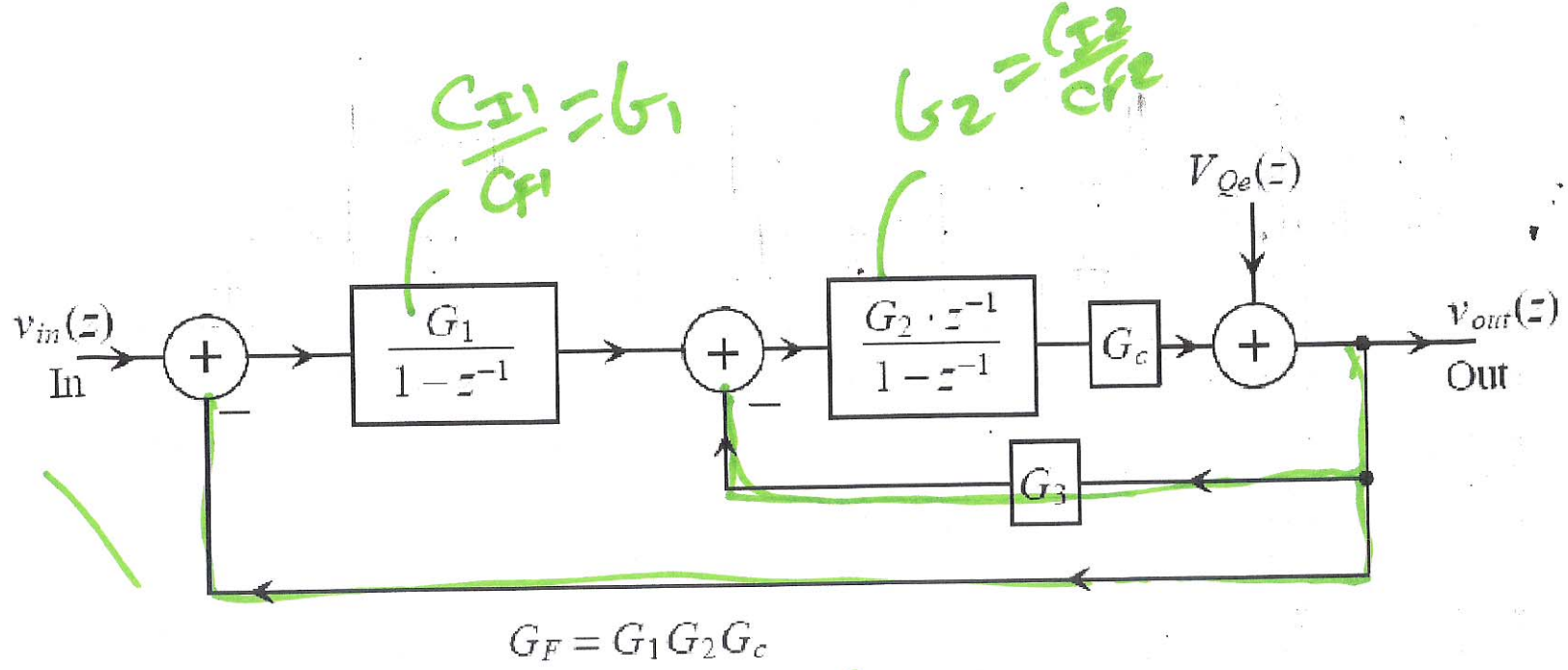
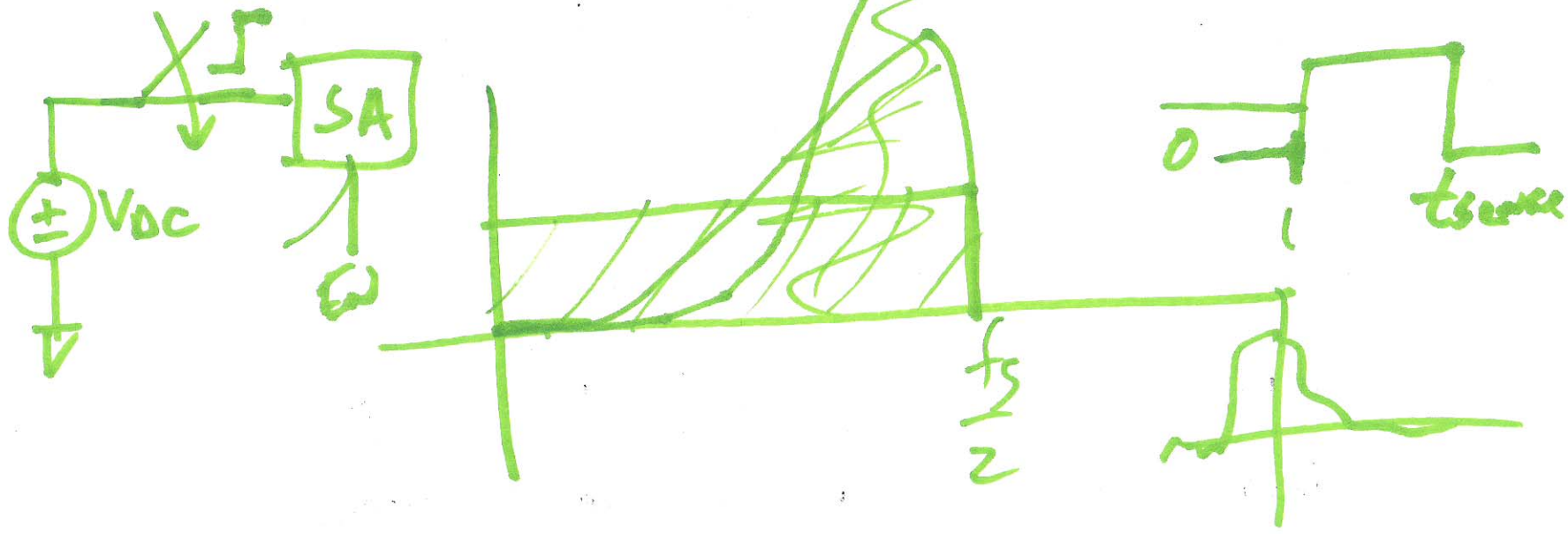


Figure 7.32. Generic block diagram of a second-order NS modulator.



8)