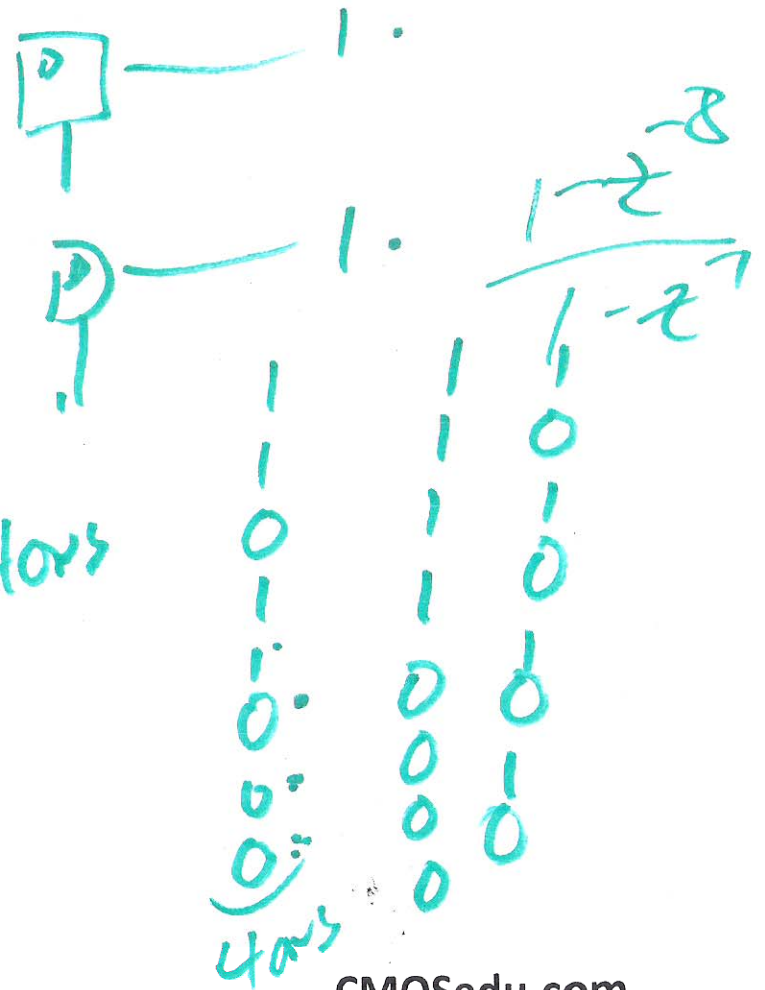


1.25ns
1.25ns
1.25ns

(1) 1 1 0 1



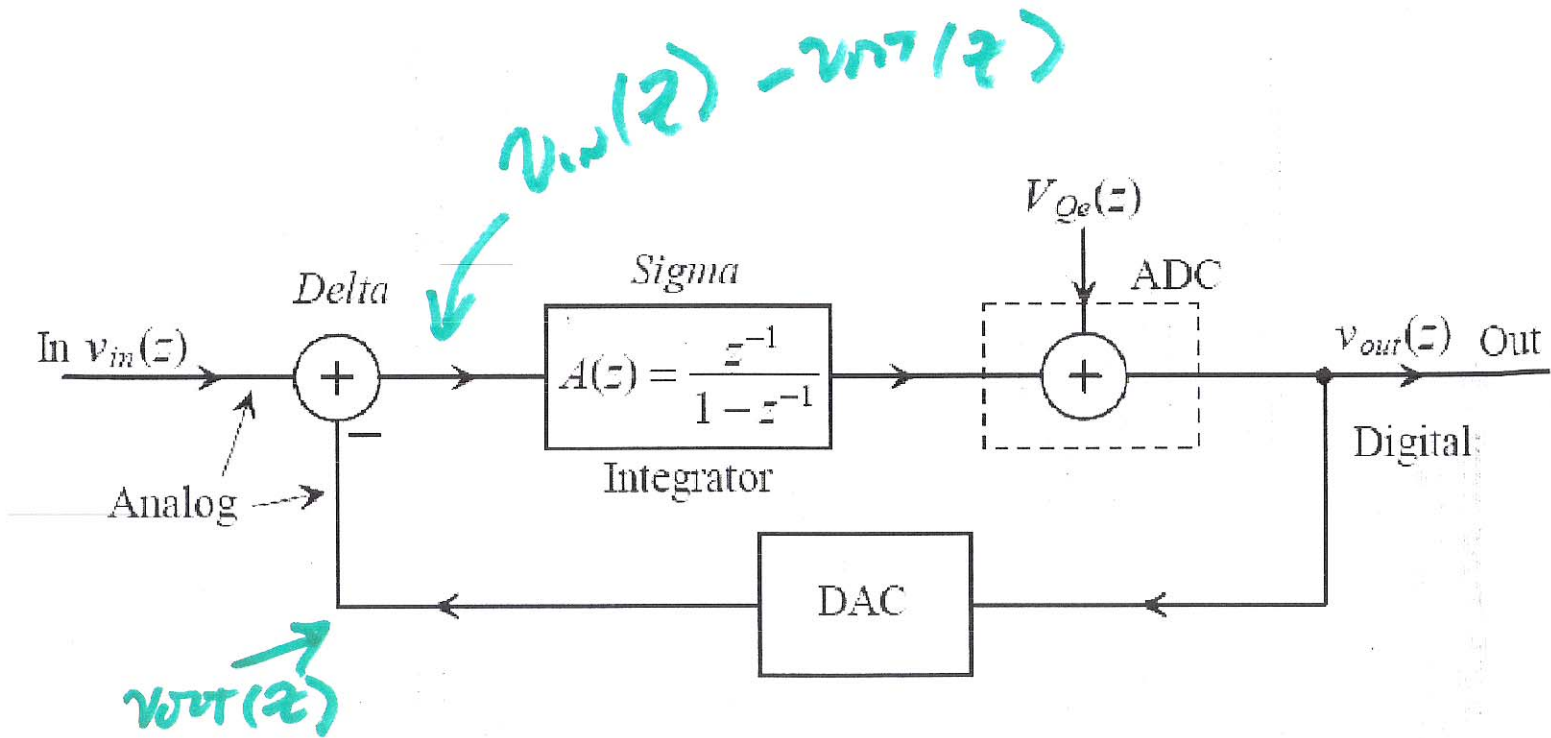


Figure 7.1 Block diagram of a noise-shaping (NS) modulator.

$$v_{out}(z) = v_{qe}(z) + \frac{z^{-1}}{1 - z^{-1}} (v_{in}(z) - v_{out}(z))$$

$$v_{out}(z)(1 - z^{-1}) = v_{qe}(z)(1 - z^{-1}) + z^{-1} v_{in}(z)$$

$$v_{out}(z) = v_{in}(z)z^{-1} + v_{qe}(z)(1 - z^{-1}) - z^{-1}v_{out}(z)$$

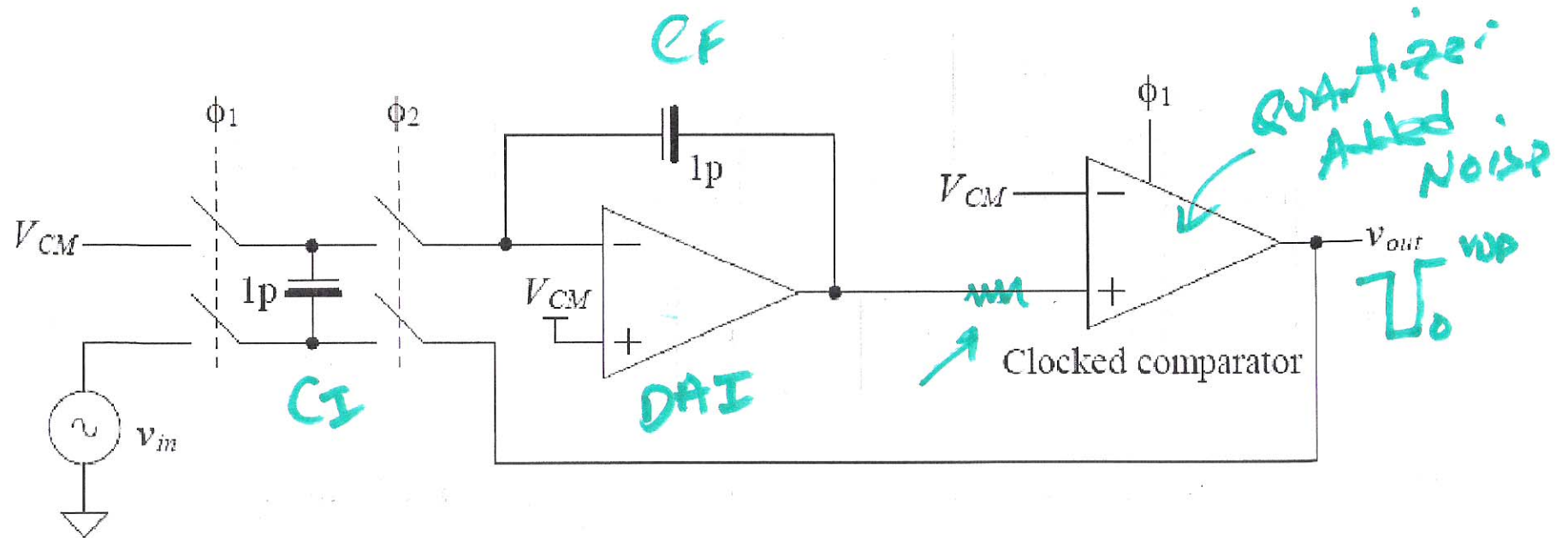


Figure 7.2 Circuit implementation of a first-order NS modulator.

$$G = \frac{C_I}{C_F} \cdot \frac{z^{-1}}{1-z^{-1}}$$

3)

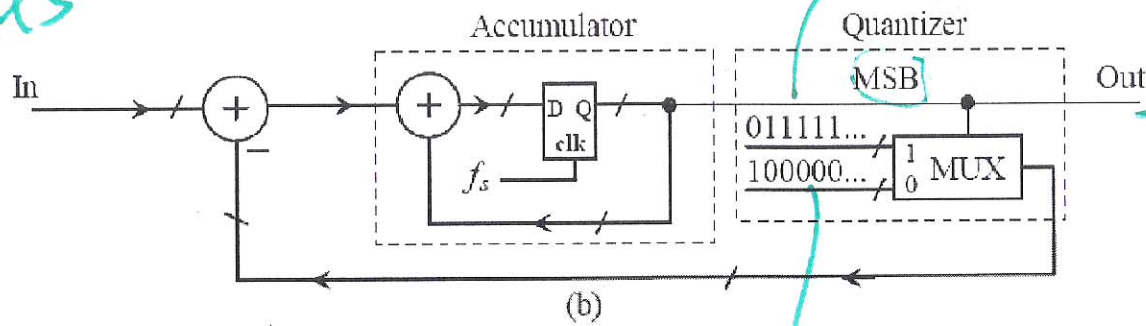
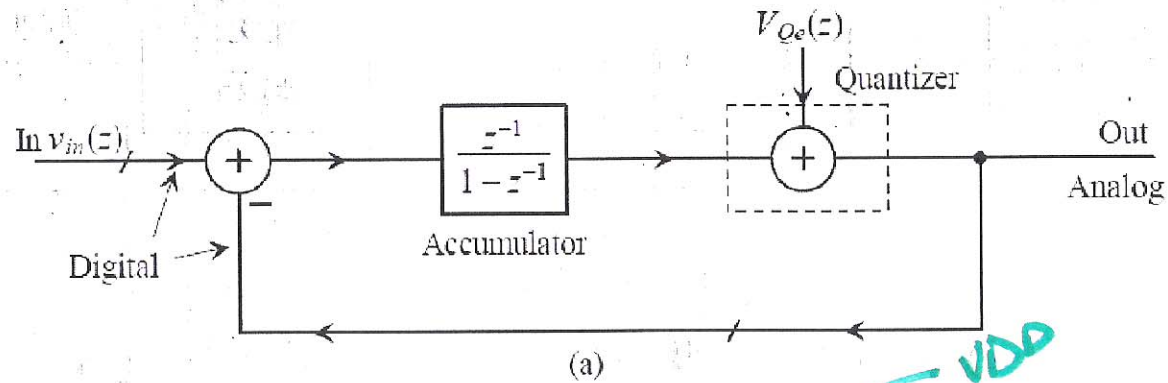


Figure 7.5 Block diagram of (a) a NS demodulator and, (b) a more detailed implementation for use in a DAC.

$$OSR = \frac{f_s}{2 \cdot f_b} = 50$$

18-bits



4)

$$V_{out}(z) = V_{in}(z^{-1}) + V_{oe}(1 - z^{-1})$$

$$V_{out}(NTs) = V_{in}((N-1)Ts) + V_{oe}(NTs)$$

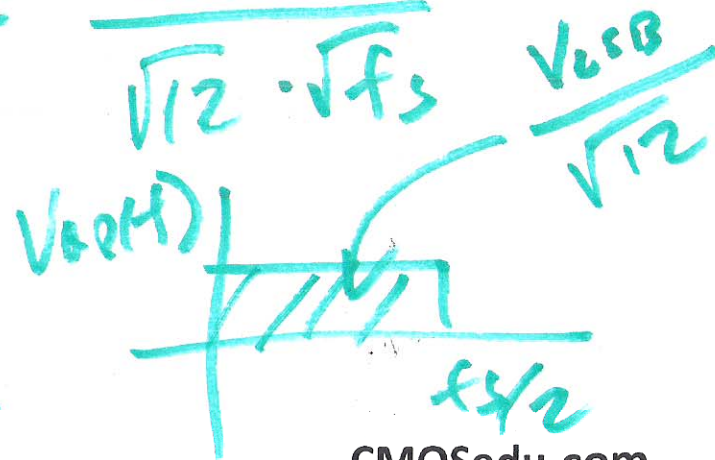
modulation noise $- V_{oe}((N-1)Ts)$

$$= NTF \cdot V_{oe}(f) = (1 - z^{-1}) V_{oe}$$

$$= (1 - e^{-j2\pi f Ts}) V_{oe}(f)$$

$$V_{oe}(f) = \frac{V_{LSB}}{\sqrt{12} \cdot \sqrt{f_s}}$$

$$|NTF(f)|^2 \cdot |V_{oe}(f)|^2 = \frac{V_{LSB}^2}{12 f_s} \cdot 4 \sin^2 \pi \frac{f}{f_s}$$



RMS modulations

$$V_{op,rms}^2 = 2 \cdot \frac{V_{LSB}^2}{12f_s} \cdot 4 \int_0^B \sin^2 \pi \frac{f}{f_s} \cdot df$$

$$\frac{f}{f_s} \ll 1 \quad \sin x \approx x$$

$$OSR = K = \frac{f_s}{2 \cdot B}, \quad B = \frac{f_s}{2K}$$

↑ oversampling ratio

$$V_{op,rms} \approx \frac{V_{LSB}}{\sqrt{12}} \cdot \frac{\pi}{\sqrt{3}} \cdot \frac{1}{K^{3/2}}$$

$$f_s = 100 \text{ MHz}$$

$$B = 6.25 \text{ MHz}$$

$$K = \frac{100 \text{m}}{2 \cdot 6.25} = 8$$

oversampling rather

$$L = M + 1$$

first-order $m = 1$

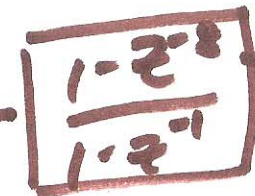
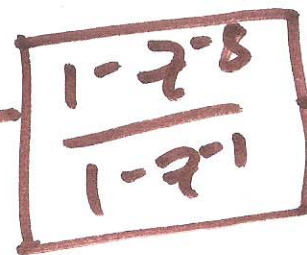
$$\left(\frac{1 - z^{-8}}{1 - z^{-1}} \right)^2$$

$$L = 2$$

Analogs



$$f_s = 100 \text{ MHz}$$



$$27 - 5.17 = 22$$

$$30 \log_2^3 - 5.17$$

$$N_{inc} =$$

$$6.02$$

$$\frac{27}{6} = 4.3$$