

EE 421 / ECL 621

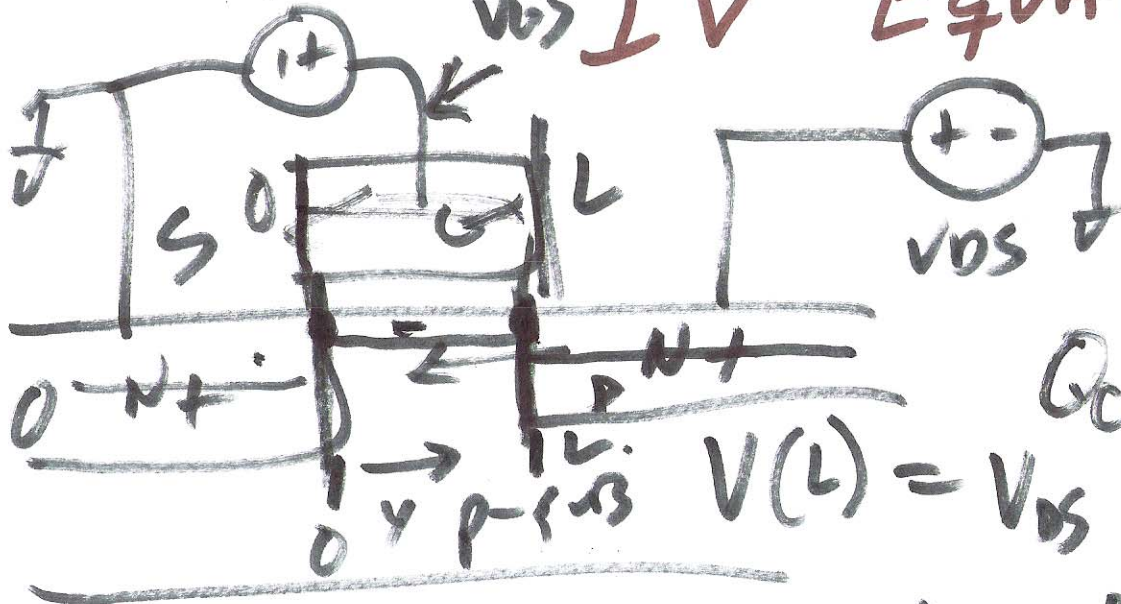
Digital IC Design

$$I_D = \frac{K_P W}{2 L} (V_{GS} - V_{THN})^2$$

OCT. 22, 2014

$$V_{GS} \geq V_{THN}$$

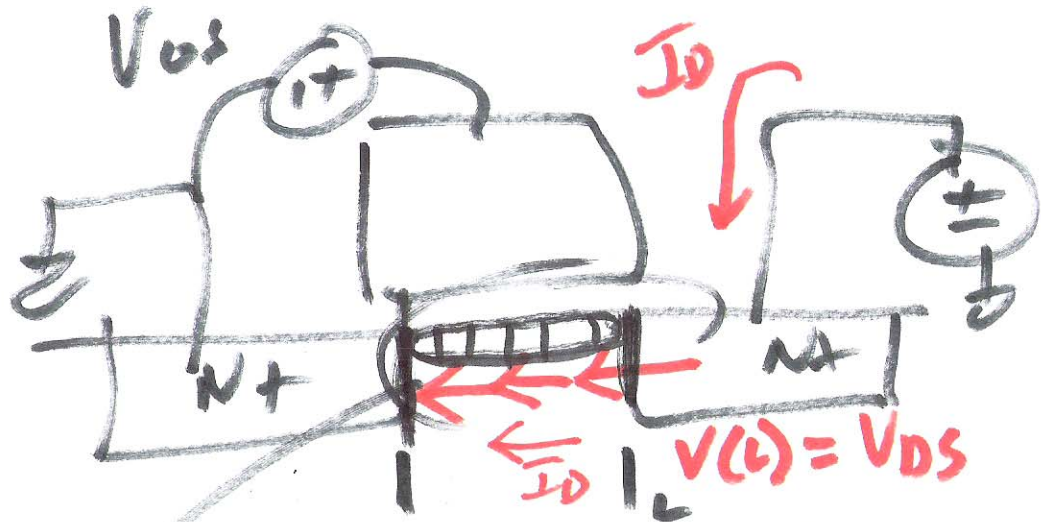
IV Equations of MOSFETS



$$Q_{CH}^{(y)} = C_{ox}' (V_{GS} - V(y))$$

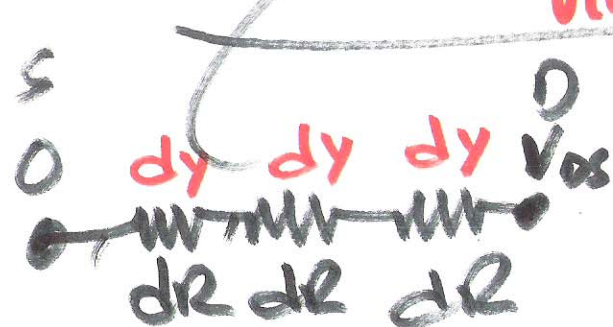
$$V(0) = 0$$

1)



$$V(0) = 0$$

$$V(L) = V_{DS}$$



$$dv = I_0 dr$$

$$Q'_{ch} = C'_{ox} (V_{GS} - V(Y))$$

$$Q'_b = C'_{it} V_{TH}$$

$$\int_0^L dy = L$$

$$dr = R_{sheet} \frac{dy}{W}$$

$$\frac{I_0}{\mu_n (Q'_{ch} - Q'_b)}$$

I_0

2)

$$\int_0^{V_{DS}} dv(y) = I_D dR = \int_0^L \frac{1}{\mu_n \cdot Q'_I(y)} \cdot \frac{dy}{W} \cdot I_D$$

$$I_D \cdot dy = \mu_n Q'_I(y) \cdot W \cdot dV(y)$$

$$= \mu_n \cdot W (Q'_{ox}(y) - Q'_s) \cdot dV(y)$$

$$I_D \cdot dy = \mu_n \cdot W (C'_{ox} (V_{DS} - V(y) - V_{THn}))$$

$$\int_0^L I_D \cdot dy = \mu_n W C'_{ox} \left(\int_0^{V_{DS}} V_{DS} dV(y) - \int_0^{V_{DS}} V(y) dV(y) - \int_0^{V_{DS}} V_{THn} dV(y) \right)$$

$$I_D \cdot L = 4.5 \mu C \alpha \left(V_{GS} \cdot V_{DS} - \frac{1}{2} V_{DS}^2 - V_{THN} V_{DS} \right)$$

$$I_D = 4.5 \mu C \alpha \frac{W}{L} \left((V_{GS} - V_{THN}) V_{DS} - \frac{1}{2} V_{DS}^2 \right)$$

$$(V_{GS} - V_{THN}) - V_{THN}$$

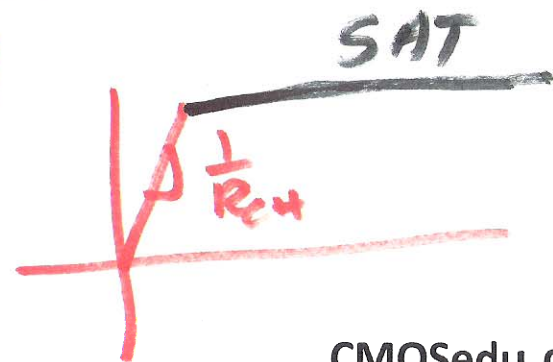
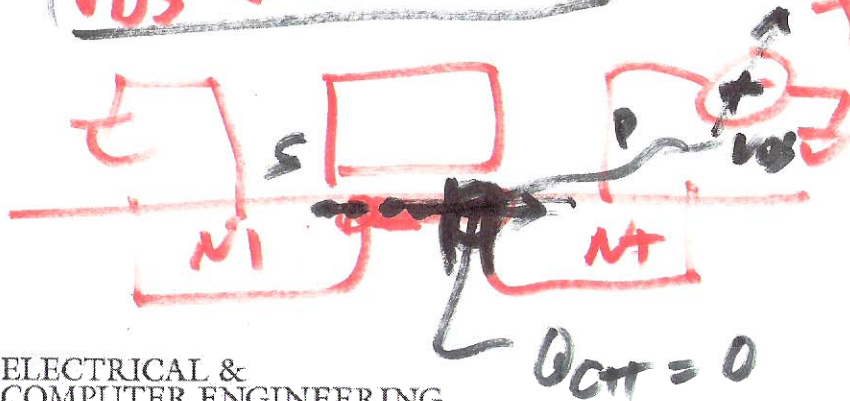
V_{DS}

$$V_{DS} < V_{GS} - V_{THN}$$

$$V_{GS} > V_{THN}$$

$$V_{DS} < V_{GS} - V_{THN}$$

for triode



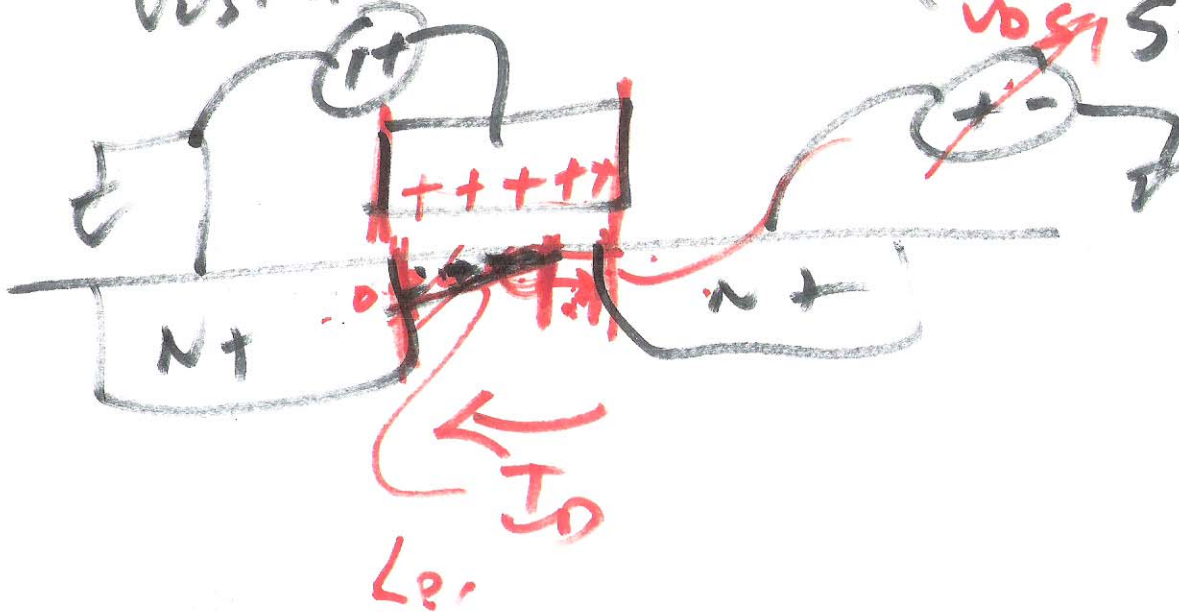
for sAT

$$V_{GS} > V_{TH}, \quad V_{DS} \geq V_{GS} - V_{TH}$$

$$I_D = \mu_n C_{ox} \frac{W}{L} \left((V_{GS} - V_{TH}) \underbrace{(V_{GS} - V_{TH})}_{V_{DS}} - \frac{(V_{GS} - V_{TH})^2}{2} \right)$$

$$\stackrel{V_{DS} > V_{TH}}{=} \frac{\mu_n C_{ox}}{2} \cdot \frac{W}{L} (V_{GS} - V_{TH})^2$$

~~$V_{DS} > V_{TH}$~~ SATURATION!



5)

for triode

$$V_{GS} > V_{THN}$$

$$V_{DS} \leq V_{GS} - V_{THN}$$

$$I_D = \mu_n C'_{ox} \cdot \frac{W}{L} \left((V_{GS} - V_{THN}) V_{DS} - \frac{V_{DS}^2}{2} \right)$$

$$K_{PN} = \mu_n C'_{ox}$$

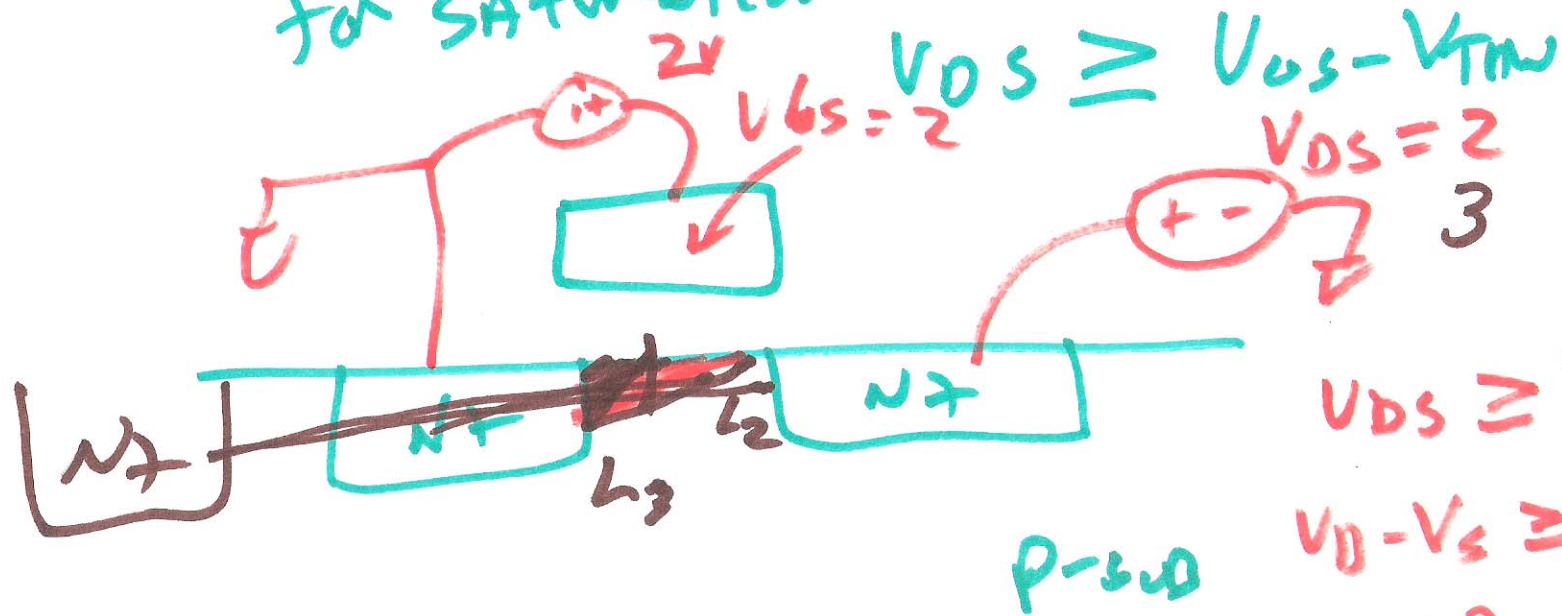
$$\beta_N = \mu_n C'_{ox} \cdot \frac{W}{L} = K_{PN} \cdot \frac{W}{L}$$

for saturation

$$C'_{ox} = \frac{\epsilon_{ox}}{t_{ox}}$$

$$\begin{aligned} I_D &= \frac{\mu_n C'_{ox}}{2} \cdot \frac{W}{L} (V_{GS} - V_{THN})^2 \\ &= \frac{K_{PN} \cdot W}{2} (V_{GS} - V_{THN})^2 \\ &= \frac{\beta_N}{2} (V_{GS} - V_{THN})^2 \end{aligned}$$

for saturation



$$V_{DS} \geq V_{GS} - V_{TH}$$

$$V_D - V_S \geq V_{GS} - V_S$$

$$V_D \geq V_G - V_{TH}$$

IN SATURATION

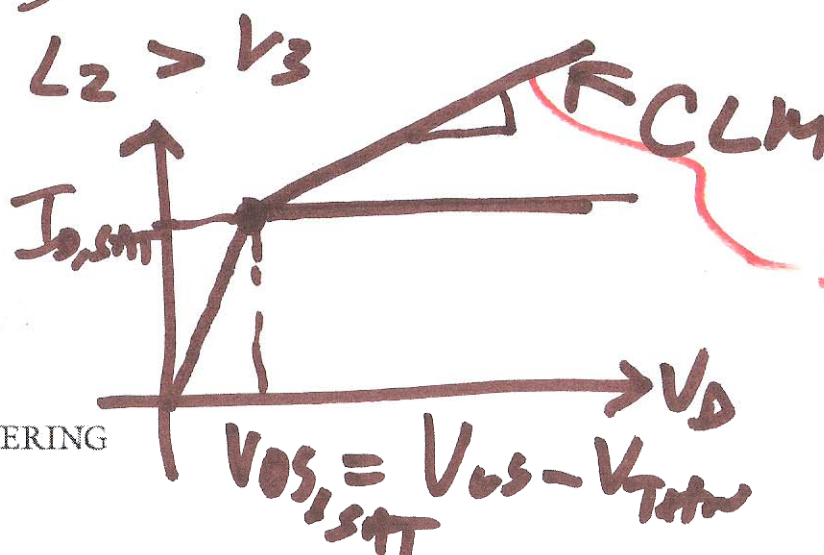
$$I_{D,sat} = \frac{K_P \cdot W}{L} (V_G - V_{TH})^2$$

$$V_{GS} \leq V_{GS,sat}$$

t. node

$$V_{DS} \geq V_{DS,sat}$$

SAT



45° ↓

$$\text{slope} = \frac{1}{\lambda I_{D,sat}}$$

$$I_D = \underbrace{\frac{\beta_N}{2} (V_{GS} - V_{THN})^2}_{I_{D,sat}} (1 + \lambda (V_{DS} - V_{DS,sat}))$$

$$I_D = I_{D,sat} (1 + \lambda ())$$

channel length modulation parameter
units = $\frac{1}{V} = V^{-1}$