

## Ch. 31.2

### Properties of feedback Amps

- 1) Gain desensitivity.
- 2) Bandwidth extension
- 3) Reduction of NON-Linear dist.
- 4) input/output impedance control

$$A_{CL} = \frac{A_{OL}}{1 + A_{OL} \cdot \beta}$$

ideally  $A_{CL} = \frac{1}{\beta}$

58:12

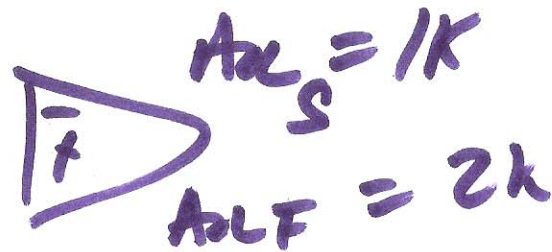
$$A_{OL1} = 10^3$$

$$A_{OL2} = 2k$$

$$A_{CL} \Big|_{\text{ideal}} = 10 = \frac{1}{\beta}$$

$$A_{CL1} =$$

$$A_{CL2} =$$



$$\frac{10^3}{1 + 10^3/10} \approx \frac{10^3}{1 + 10^2} \approx 10$$

$$\frac{2 \cdot 10^3}{1 + 2 \cdot 10^3/10} \approx 10$$

### 31.2.1 Gain Desensitivity

$$\frac{dA_{CL}}{dA_{OL}} = \frac{1}{dA_{OL}} \left( A_{OL} (1 + \beta A_{OL})^{-1} \right)$$
$$\frac{1}{1 + \beta A_{OL}} + \frac{-A_{OL}}{(1 + \beta A_{OL})^2} \cdot \beta$$

$$\frac{dA_{CL}}{dA_{OL}} = \frac{1 + \beta A_{OL}}{(1 + \beta A_{OL})^2} - \frac{\beta A_{OL}}{(1 + \beta A_{OL})^2}$$

$$\frac{dA_{CL}}{dA_{OL}} = \frac{1}{(1 + \beta A_{OL})^2} \quad (31.8)$$

$$\frac{dA_{CL}}{A_{CL}} = \frac{dA_{OL}}{(1 + \beta A_{OL})^2} \cdot \frac{1 + \beta A_{OL}}{A_{OL}}$$

$$\frac{100\%}{1 + \frac{1}{10} \cdot 10^3}$$

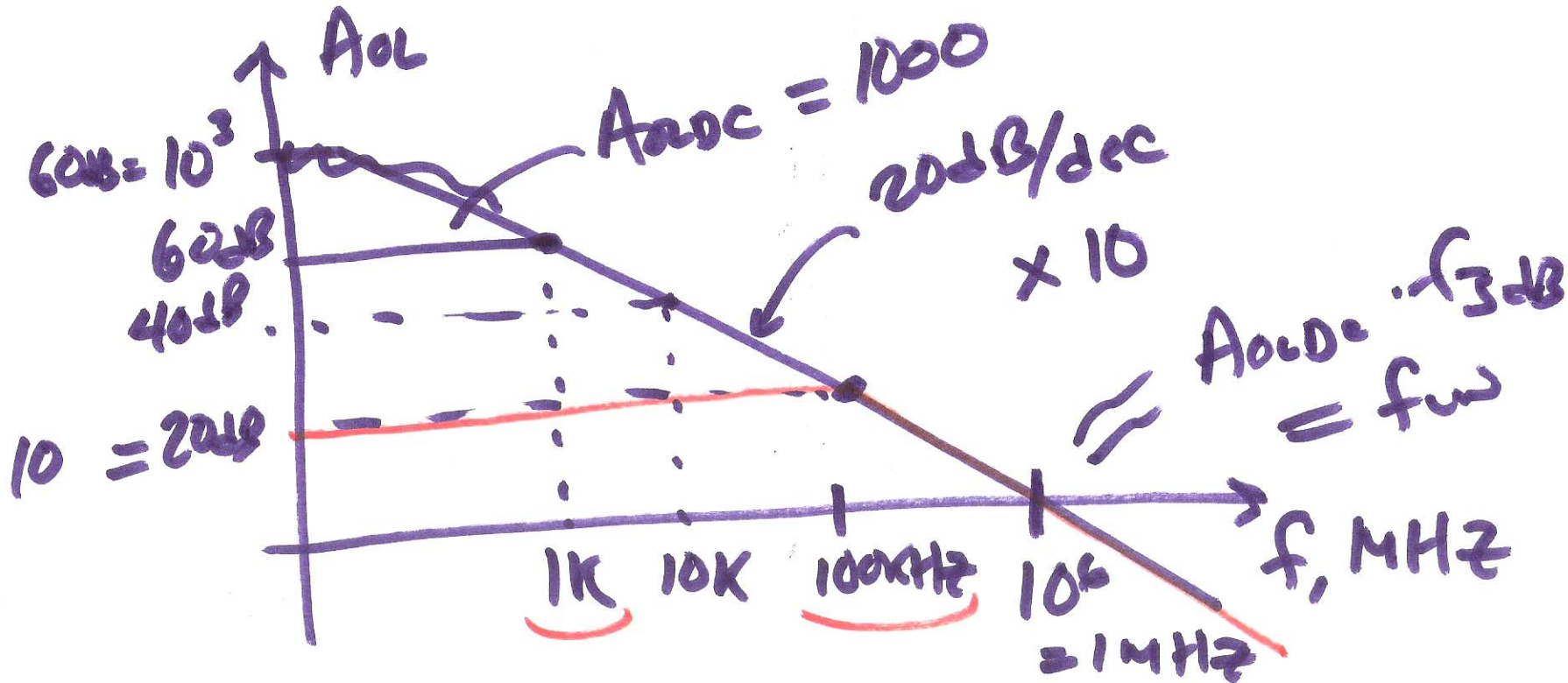
$$\leftarrow \frac{dA_{CL}}{A_{CL}} = \frac{dA_{OL}}{A_{OL}} \cdot \frac{1}{1 + \beta A_{OL}}$$

$\approx 1\%$

$$dA_{OL} = 2K - 1K = 1K$$

$$A_{OL} = 1K$$





$$A_{OL}(f) = \frac{A_{OLDC}}{1 + j \frac{f}{f_{3dB}}}$$

$$| | = \left| \frac{A_{OLDC}}{j \frac{f_u}{1000K}} \right|$$

1K

$$A_{OLDC} \cdot f_{3dB} = f_u$$

4)

$$A_{OL}(f) = \frac{A_{OLDC}}{1 + j \frac{f}{f_{3dB}}} \quad , \quad \frac{f}{f_{3dB}} = 1$$

$$A_{OL}(s) = \frac{A_{OLDC} \cdot \omega_H}{\omega_H + s}$$

$$\omega_H = 2\pi f_{3dB}$$

$$A_{OL} = \frac{A_{OLDC}}{1 + \frac{s}{\omega_H}} \quad 31.10$$

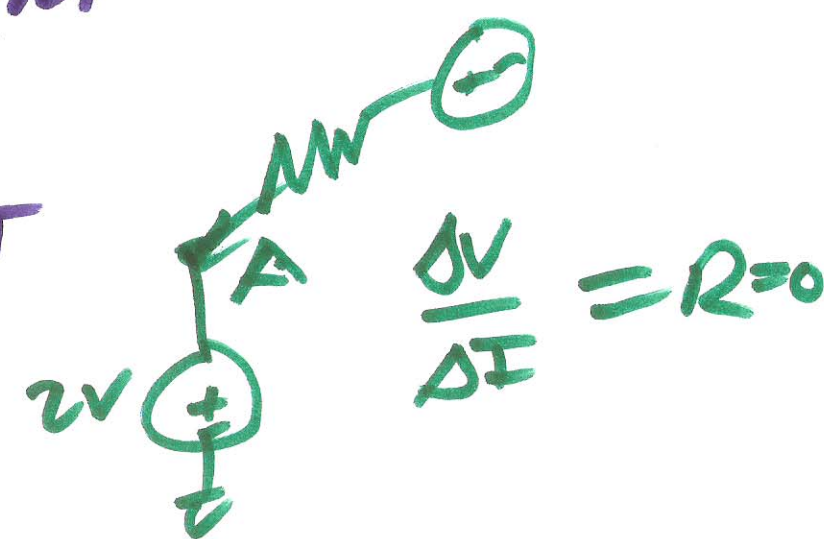
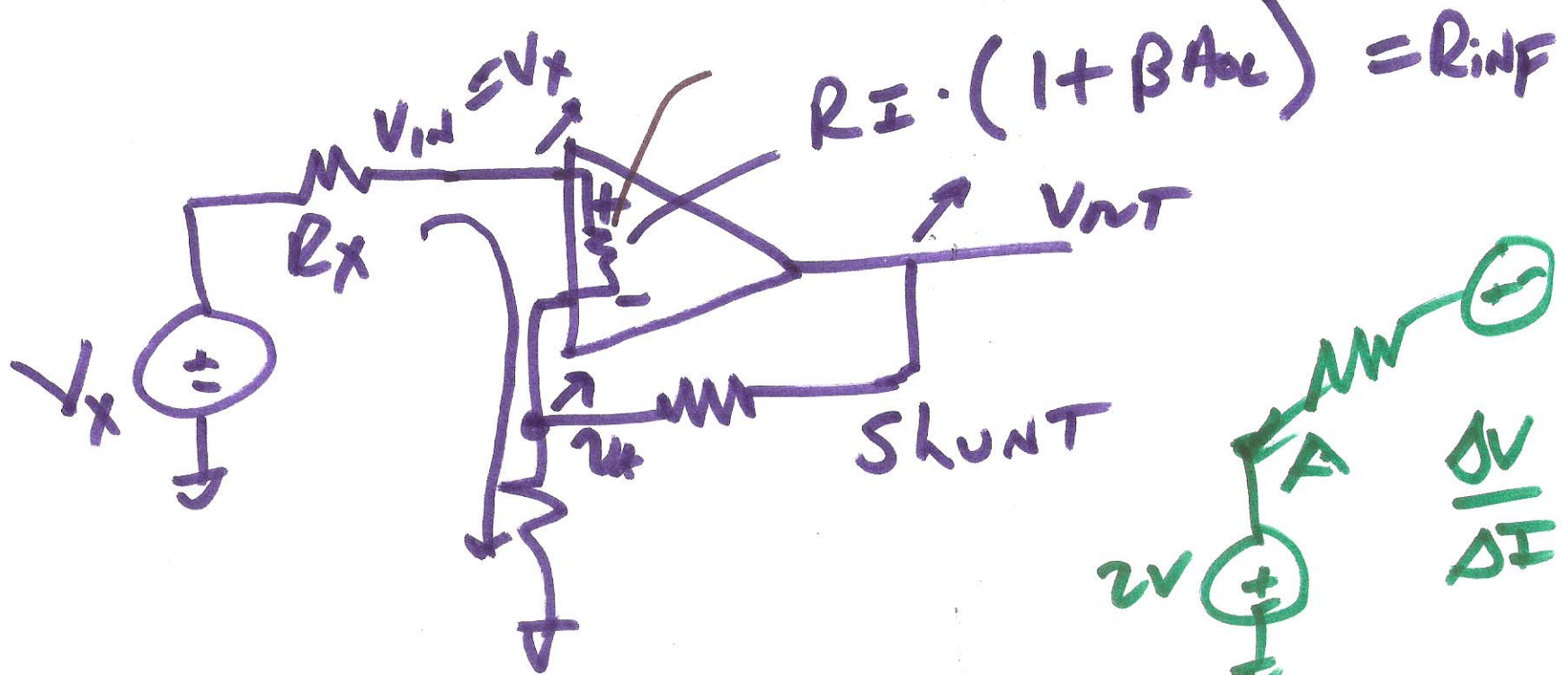
5)

$$A_{CL}(f) = \frac{A_{OLDC}}{1 + j \frac{f}{f_{3dB}}} \cdot \frac{1}{1 + \beta \frac{A_{OLDC}}{1 + j \frac{f}{f_{3dB}}}}$$

$$= \frac{A_{OLDC}}{1 + j \frac{f}{f_{3dB}} + \beta A_{OLDC}}$$

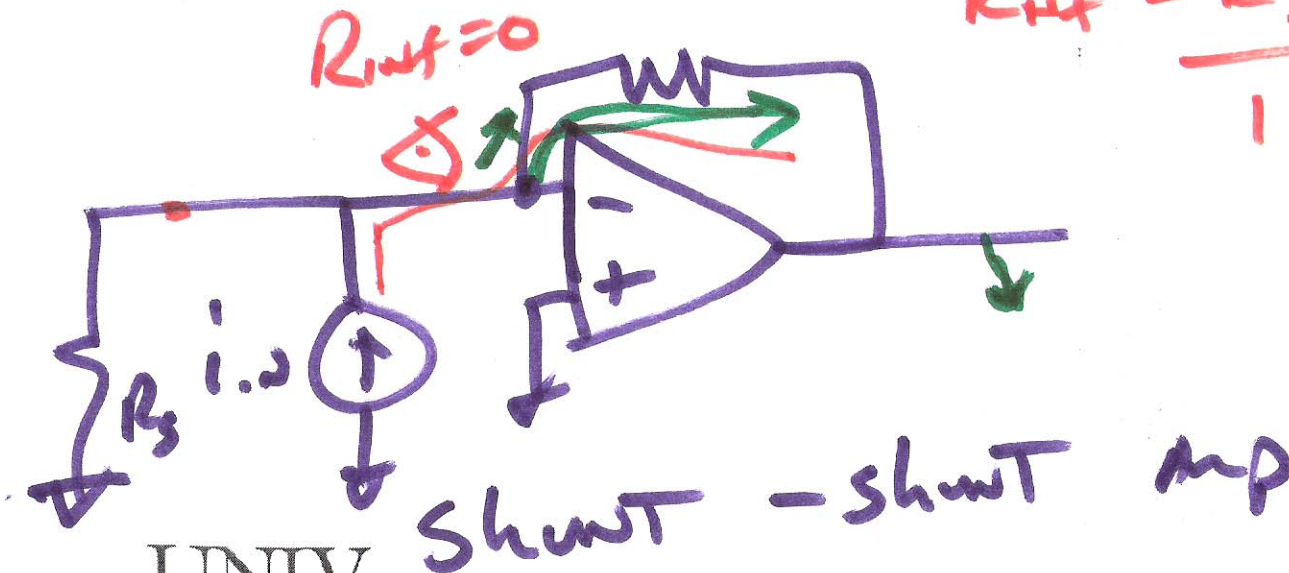
$$1 + \beta A_{OLDC} = \frac{f_{3dBCL}}{f_{3dB}}$$

$$f_{3dB}(1 + \beta A_{OLDC}) = f_{3dBCL}$$



SERIES

$R_{inF} = \frac{R_f}{1 + \beta A_{cl}}$

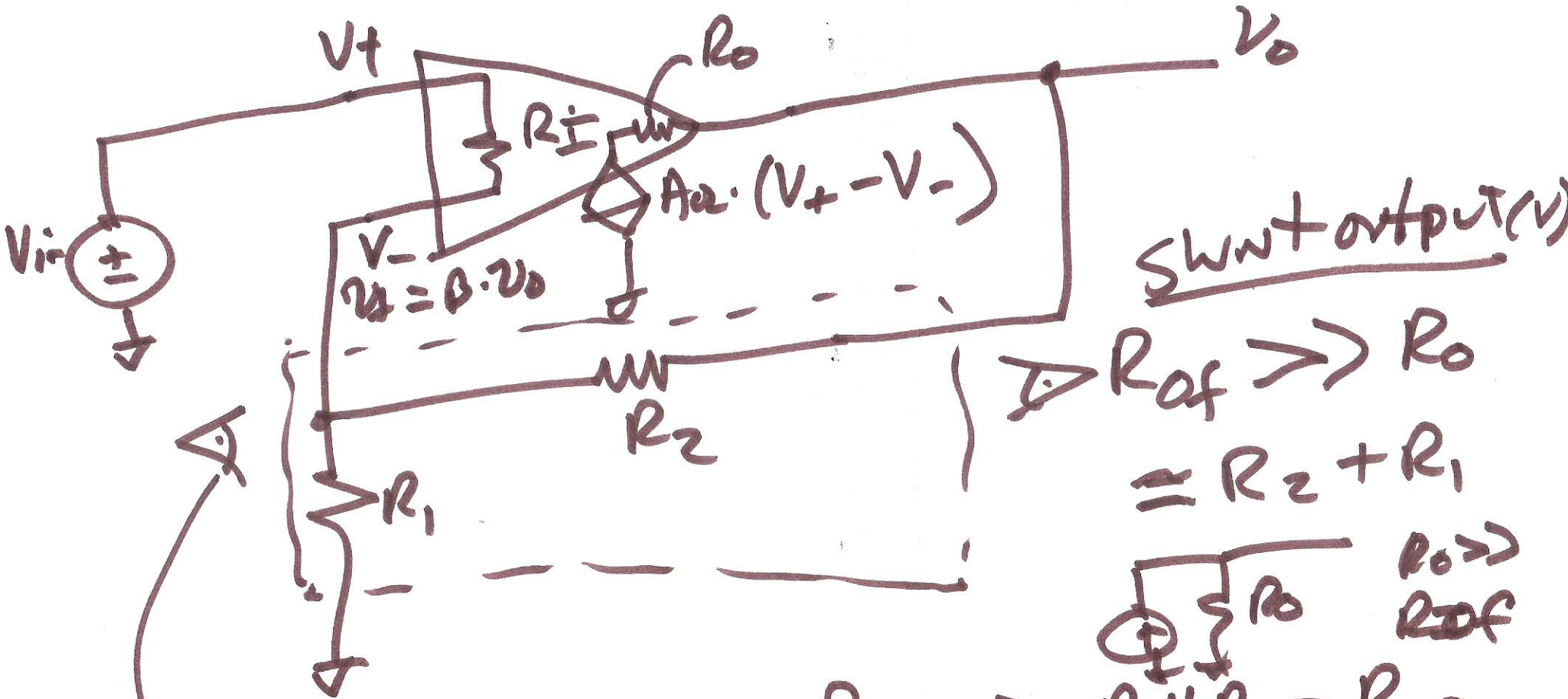


TRANSIMPEDANCE  $\frac{V_o}{I_{in}}$

GAIN =  $\Omega$

7)





Shunt output (v)

$R_{of} \gg R_o$   
 $\approx R_2 + R_1$



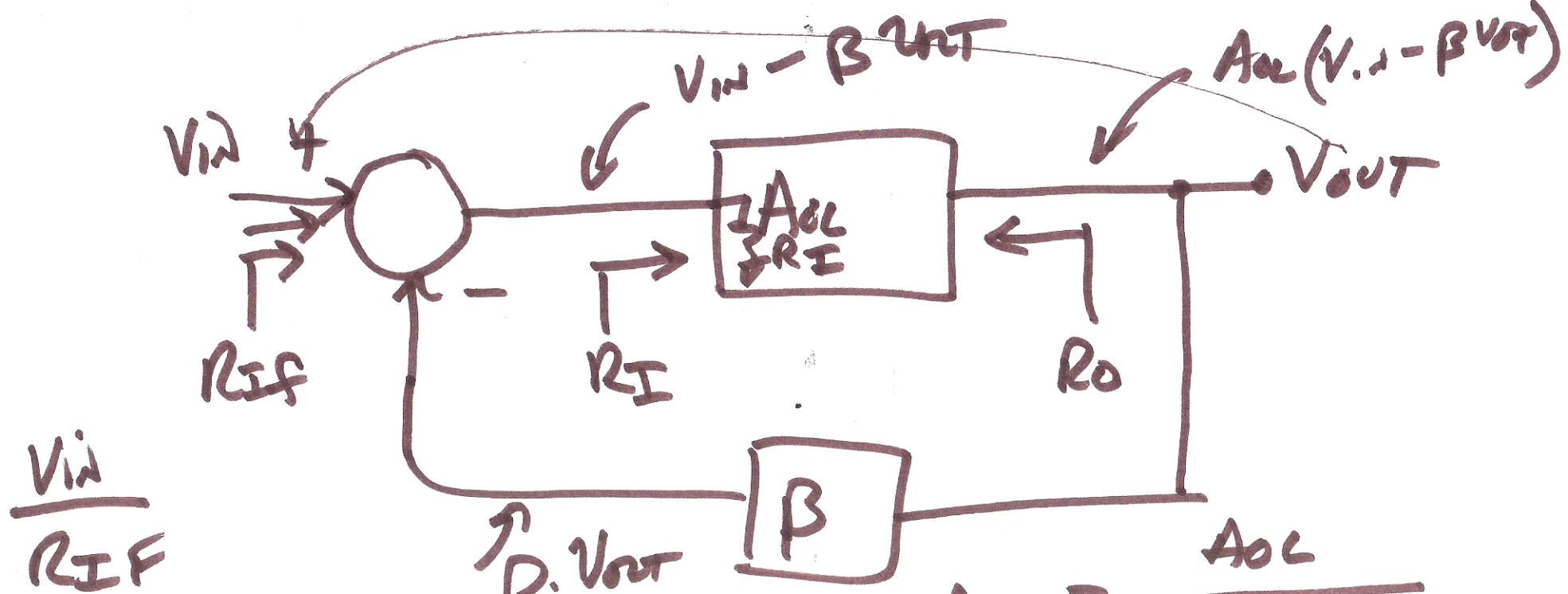
$R_{if} = R_1 \parallel R_2$   
Shunt input  
 $R_i \gg R_{if}$

$R_i \gg R_1 \parallel R_2 = R_{if}$   
series input  
 $R_i \ll R_{if}$

NOT loading Amp with f.b.

8)





$$A_{CL} = \frac{V_{out}}{V_{in}} = \frac{A_{OL}}{1 + \beta A_{OL}}$$

$$A_{CL} = \frac{V_{out}}{V_{in}} = \frac{A_{OL}}{1 + \beta A_{OL}}$$

$$V_{in} = \frac{V_{out} (1 + \beta A_{OL})}{A_{OL}}$$

$$\frac{V_{in}}{R_I} = \frac{V_{out}}{R_I} \frac{V_{in}}{R_{IF}}$$

9)

$$I = \frac{V_{in} - \beta V_{out}}{R_I}, \quad V_{out} = V_{in} \left( \frac{A_{OL}}{1 + \beta A_{OL}} \right)$$

~~$$V_{in} = \frac{\beta A_{OL} V_{in}}{(1 + \beta A_{OL}) R_I}$$~~

$$I = \frac{V_{in} - \beta \left( V_{in} \frac{A_{OL}}{1 + \beta A_{OL}} \right)}{R_I}$$

$$R_{IF} = \frac{V_{in} R_I}{V_{in} \left( \frac{1 + \beta A_{OL} - \beta A_{OL}}{1 + \beta A_{OL}} \right)}$$

$$R_{IF} = R_I (1 + \beta A_{OL})$$

$$I_I = \frac{V_{IN} - \beta V_{OUT}}{R_I}$$

$$R_{IF} = \frac{V_{IN}}{I_I}$$

$$V_{IN} \cdot \frac{A_{OL}}{1 + \beta A_{OL}} = V_{OUT}$$

$$I_{I^*} = \frac{1}{R_I} \left( V_{IN} - \frac{\beta V_{IN} A_{OL}}{1 + \beta A_{OL}} \right)$$

$$R_I (1 + \beta A_{OL}) = R_{IF} = \frac{V_{IN}}{\frac{V_{IN}}{R_I} \left( 1 - \frac{\beta A_{OL}}{1 + \beta A_{OL}} \right)}$$

$$= \frac{R_I}{\frac{1 + \beta A_{OL}}{1 + \beta A_{OL}} - \frac{\beta A_{OL}}{1 + \beta A_{OL}}}$$

11)