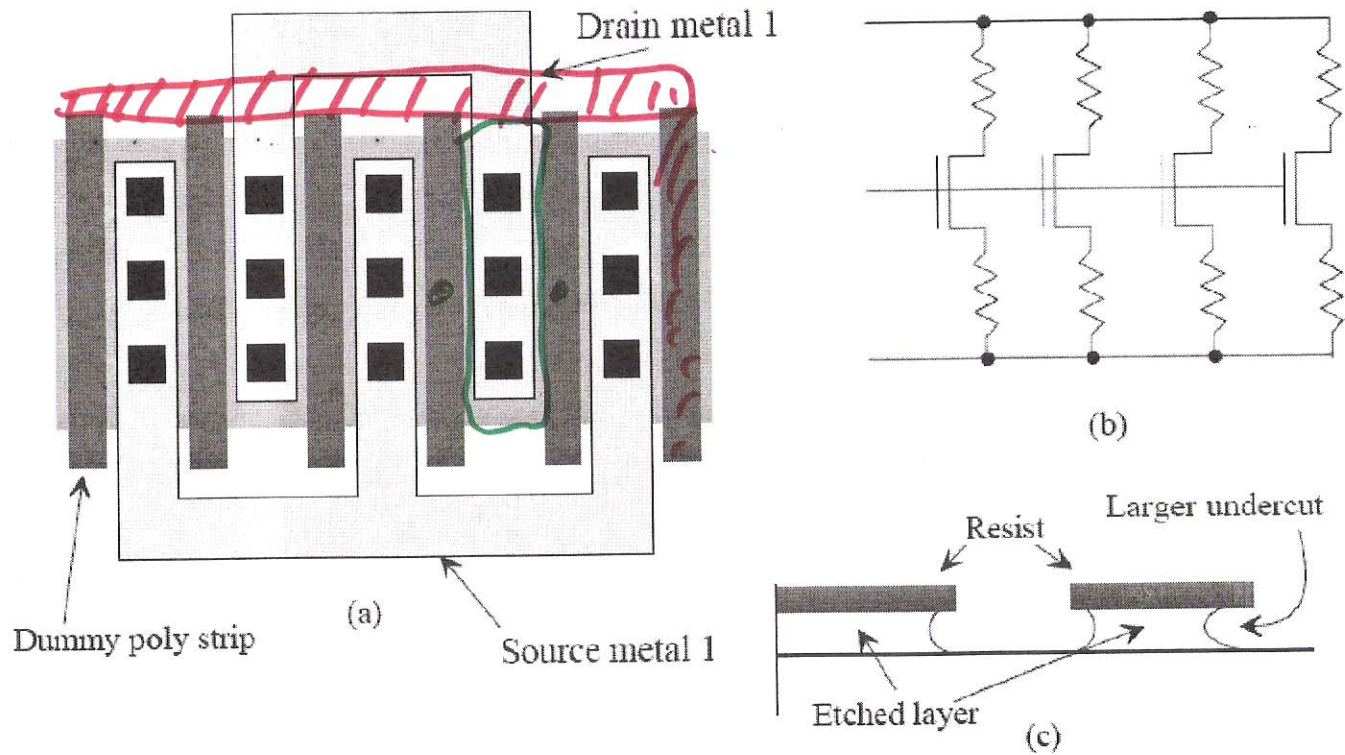


**Figure 20.5** (a) Large device with a single contact and (b) its equivalent circuit.  
 (c) Adding more contacts to reduce parasitic resistance.



**Figure 20.6** (a) A parallel device with dummy strips, (b) the equivalent circuit, and (c) undercutting.

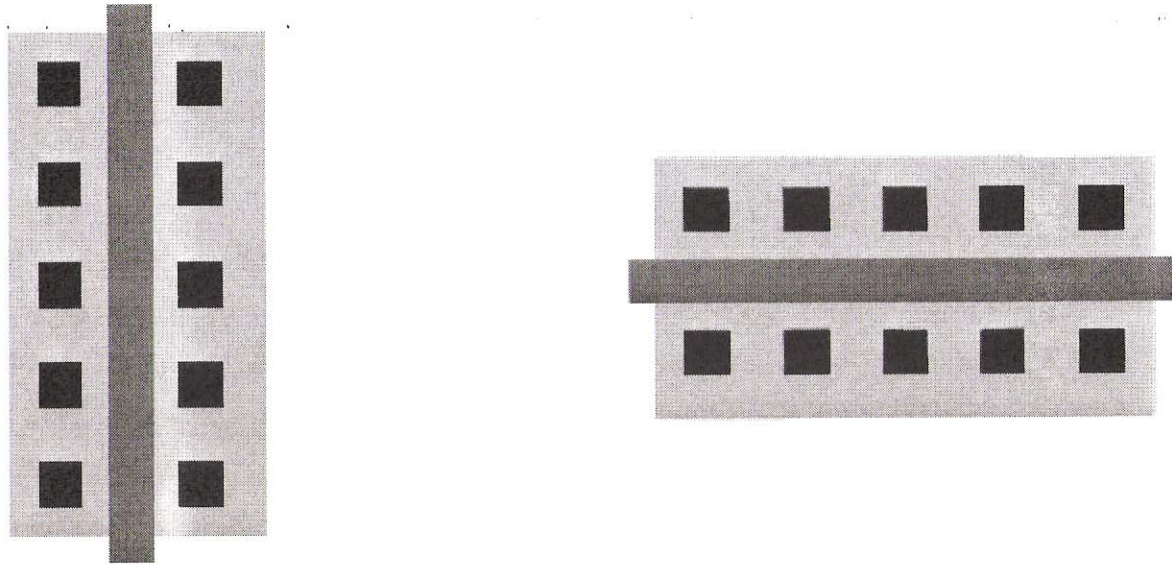
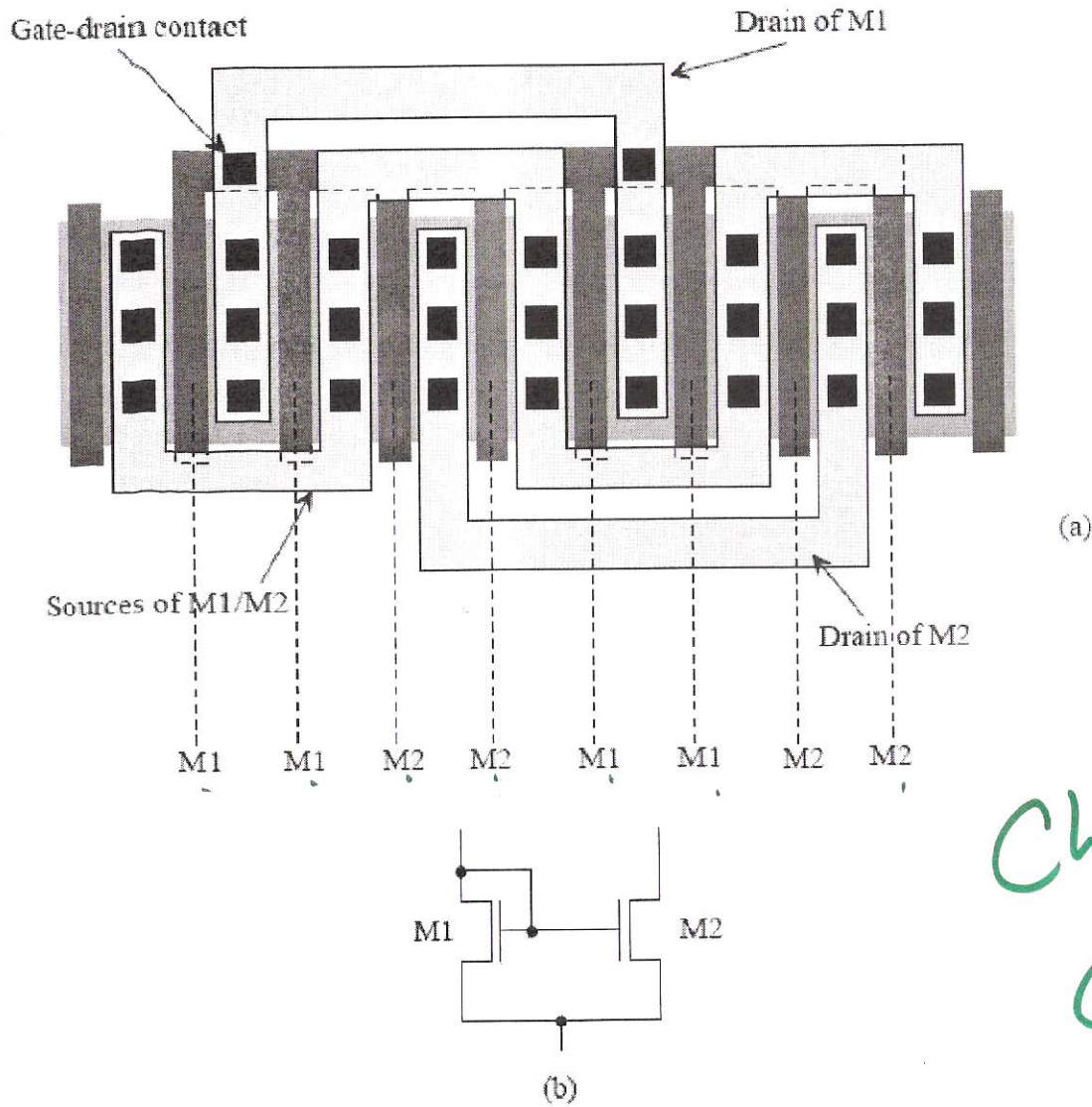


Figure 20.7 Devices with differing orientation (bad).

WANT, for good matching, devices  
to have same orientation.  
you also WANT devices  
to be close

3)



Ch. 5  
Common-Centroid  
Layout

Figure 20.8 (a) Layout of a simple current mirror using interdigitation and (b) equivalent circuit.

4)

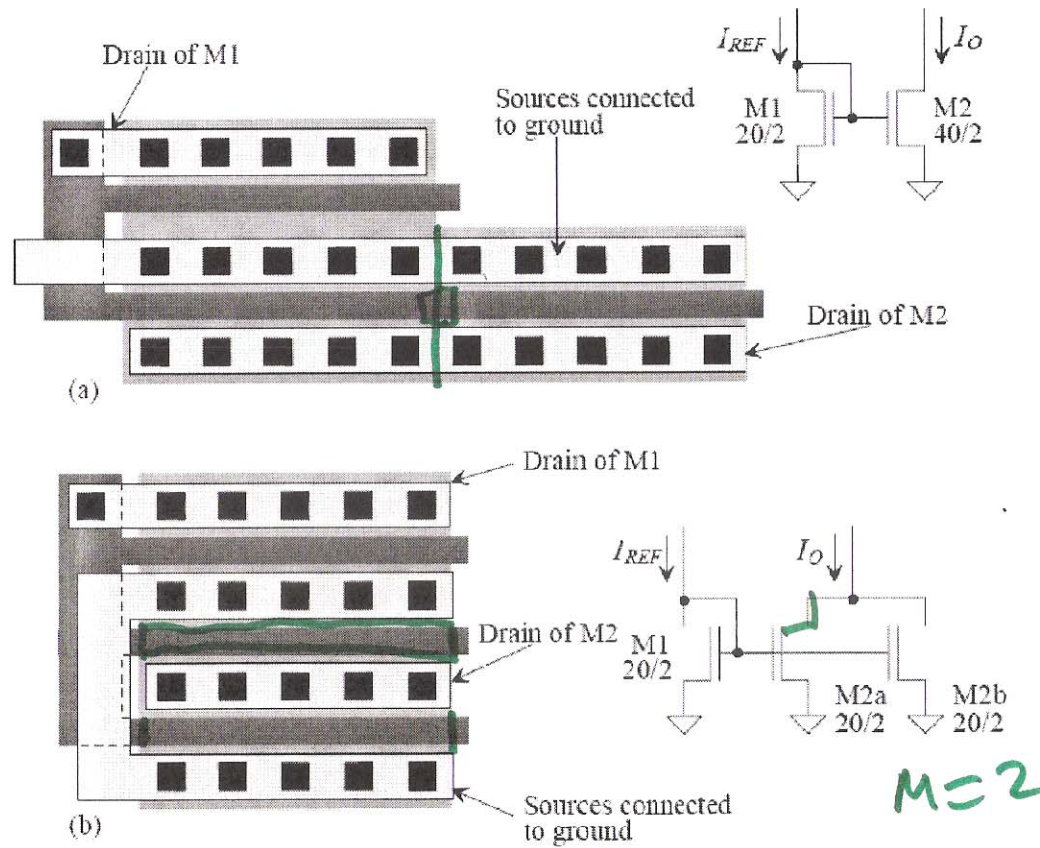


Figure 20.9 Layout of a current mirror (a) without width correction and (b) with width correction.



Sec. 20.1.3

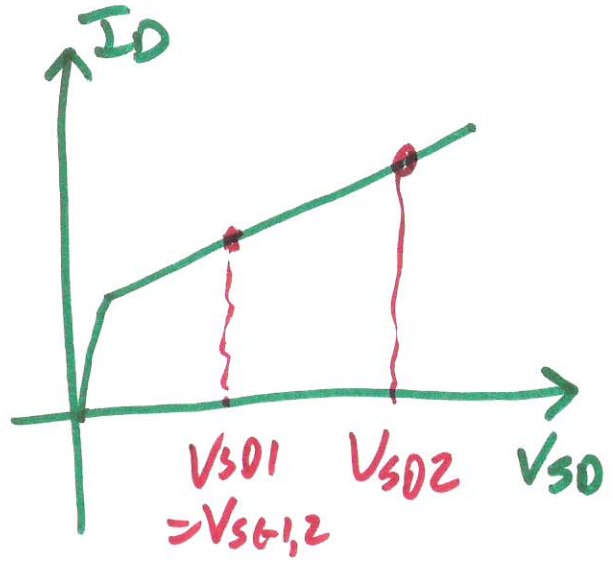
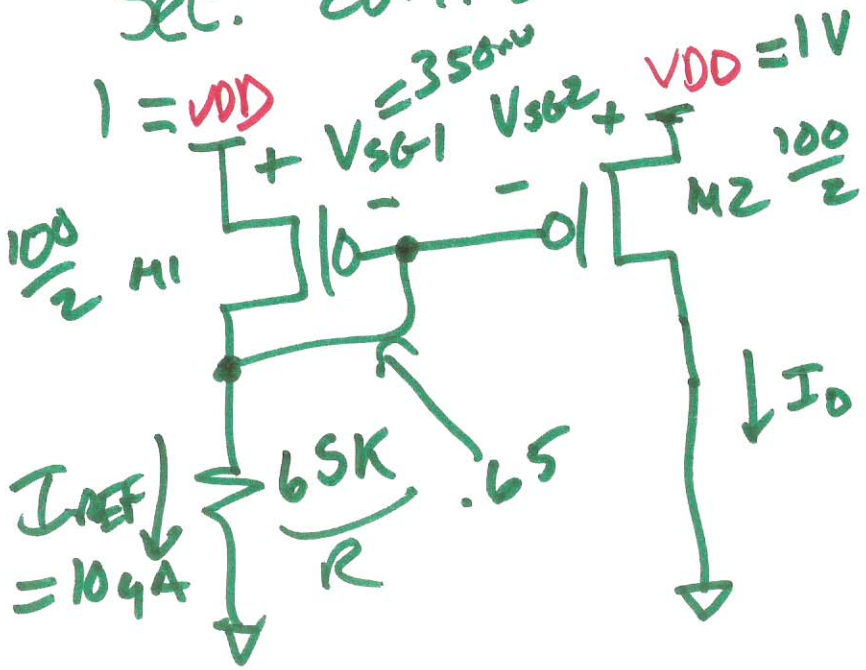
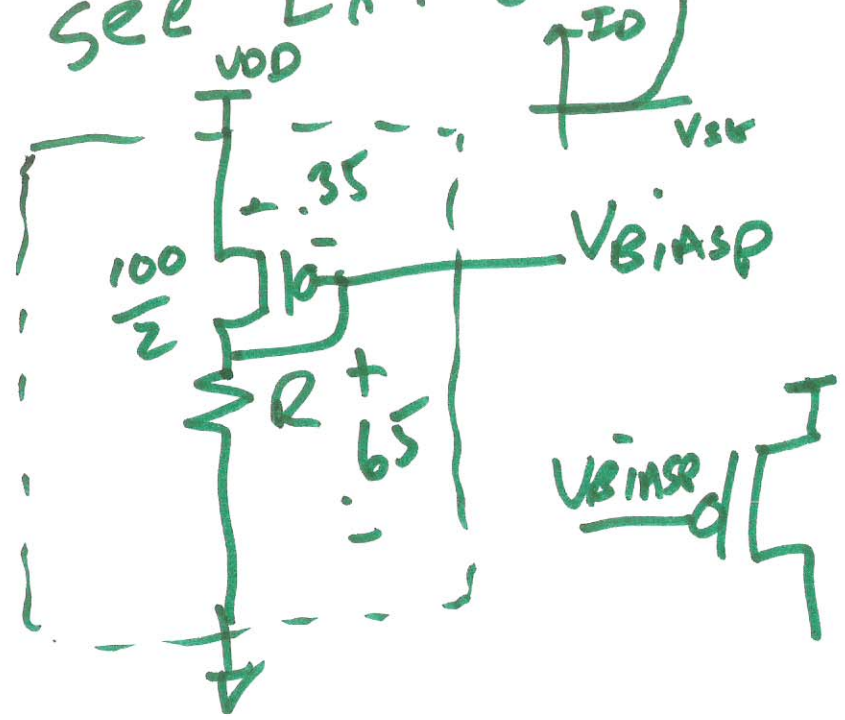


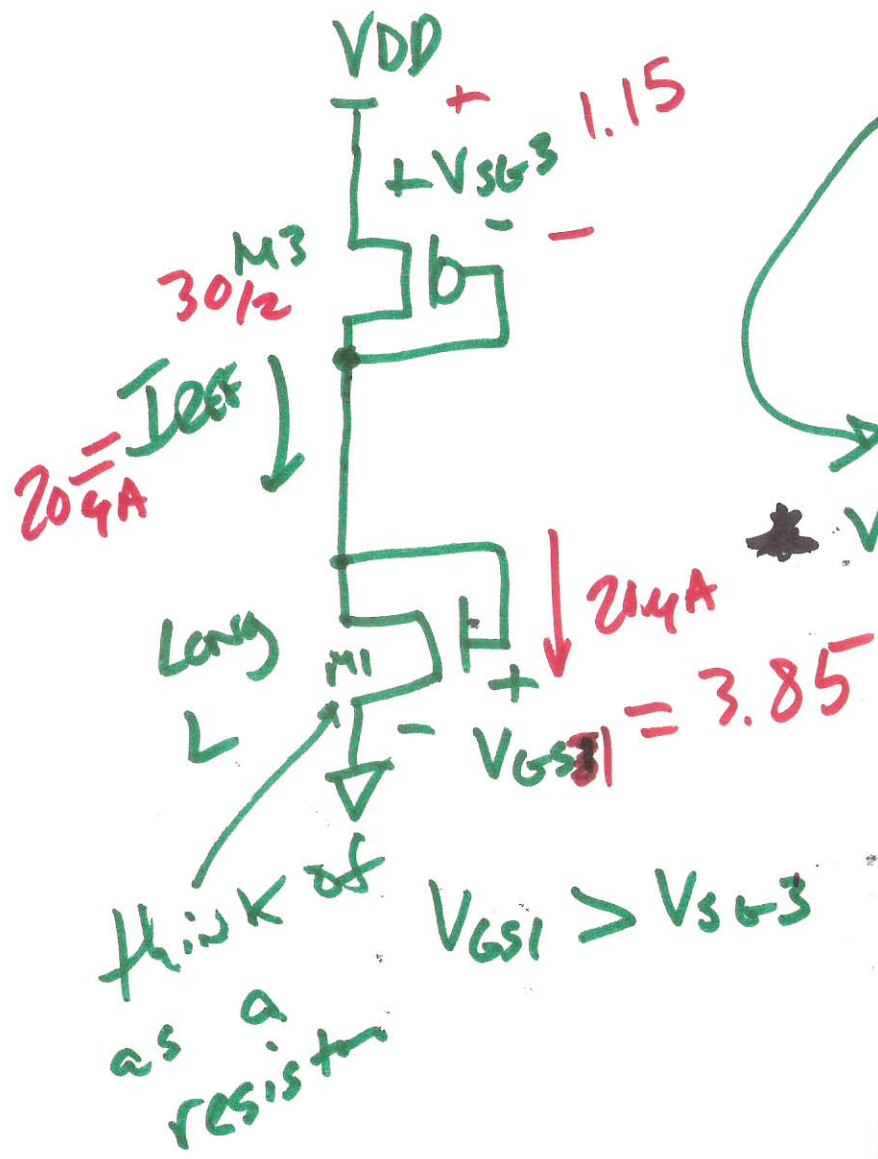
TABLE 9.2  
SCALE = 50n  
SM/100nm

$$\frac{1 - .35}{65K} = 104A$$

see Ex. 20.2



6)



$$V_{DD} = V_{sg3} + V_{gs1}$$

$$V_{gs} = \sqrt{\frac{2I_D}{K_{PN} \cdot \frac{W}{L}}} + V_{THN}$$

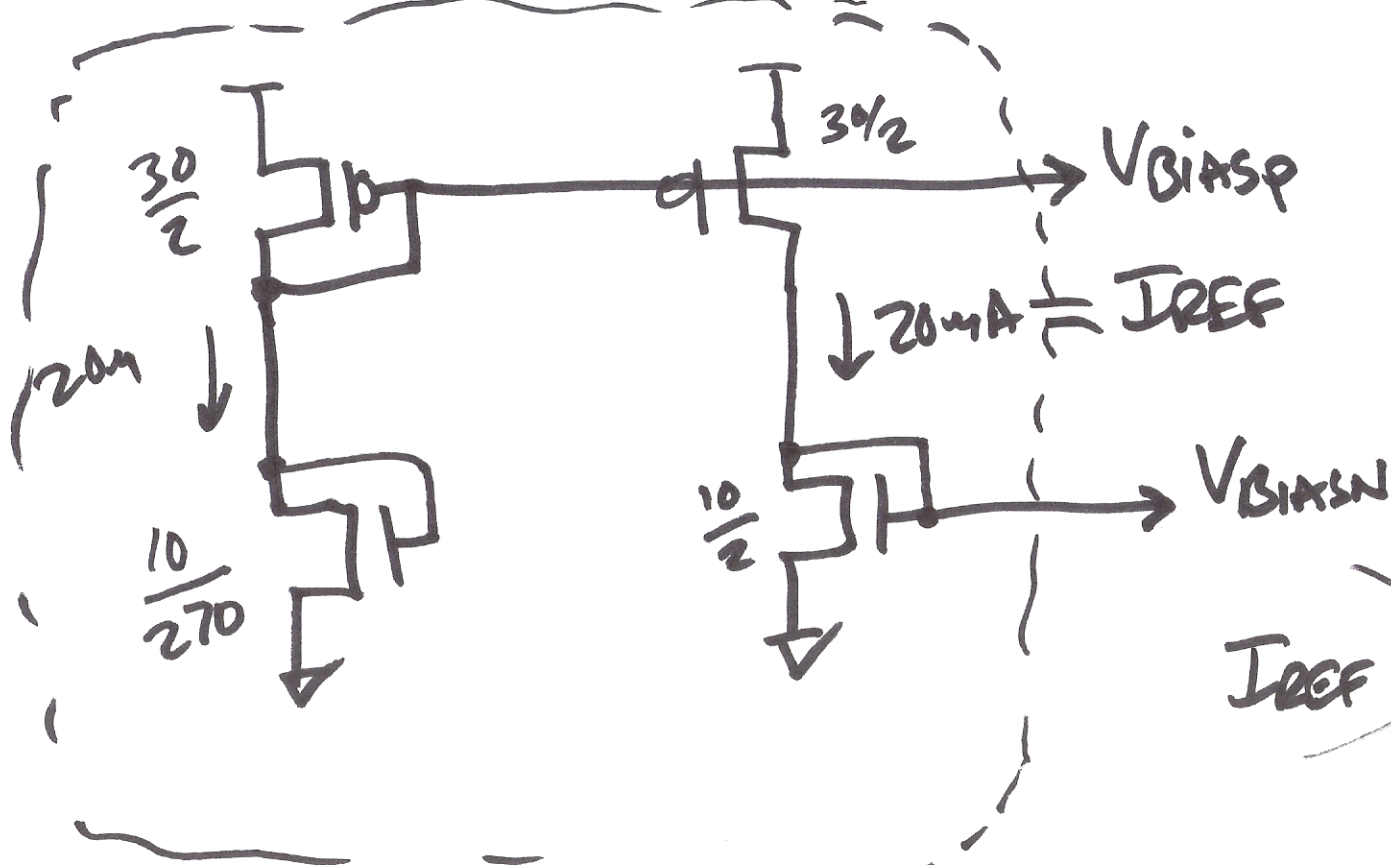
$$V_{DD} = \sqrt{\frac{2I_{REF}}{K_{PN} \cdot \frac{W_1}{L_1}}} + V_{THN} + \sqrt{\frac{2I_{REF}}{K_{PN} \cdot \frac{W_3}{L_3}}} + V_{THP}$$

3.85  
 .8  
 30/12  
 1.15

$$\sqrt{\frac{2 \cdot 204}{1204 \cdot \frac{W_1}{L_1}}} + .8 = 3.85$$

$$\frac{W_1}{L_1} \approx \frac{10}{270}$$

7)



~~$$I_{REF} = \frac{\beta_p}{2} (V_{DD} - I_{REF})$$~~

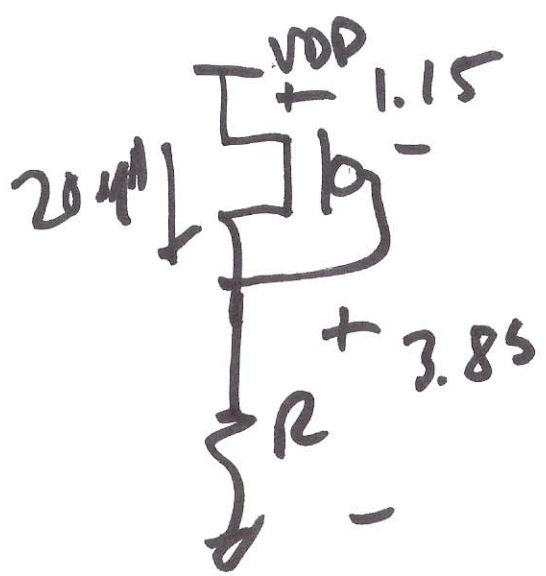
How sensitive is  $I_{REF}$  to changes in  $V_{DD}$ ?

$$\frac{\delta I_{REF}}{\delta V_{DD}} = \frac{\delta I}{V_{DD}} = \frac{2V_{DD}}{K} - \frac{2(V_{THp} + |V_{THn}|)}{K}$$

$$\frac{\delta I_{REF}}{\delta V_{DD}} = \frac{12nA}{mV}$$

8)





Long channel

$$R = \frac{3.85}{204} \approx 192K$$



$$I_{REF} = \frac{V_{DD} - |V_{th}| - V_{SG}}{R}$$

~~$$I_{REF} = \frac{V_{DD}}{R}$$~~

~~$$I_{REF} = \frac{V_{DD}}{2R}$$~~

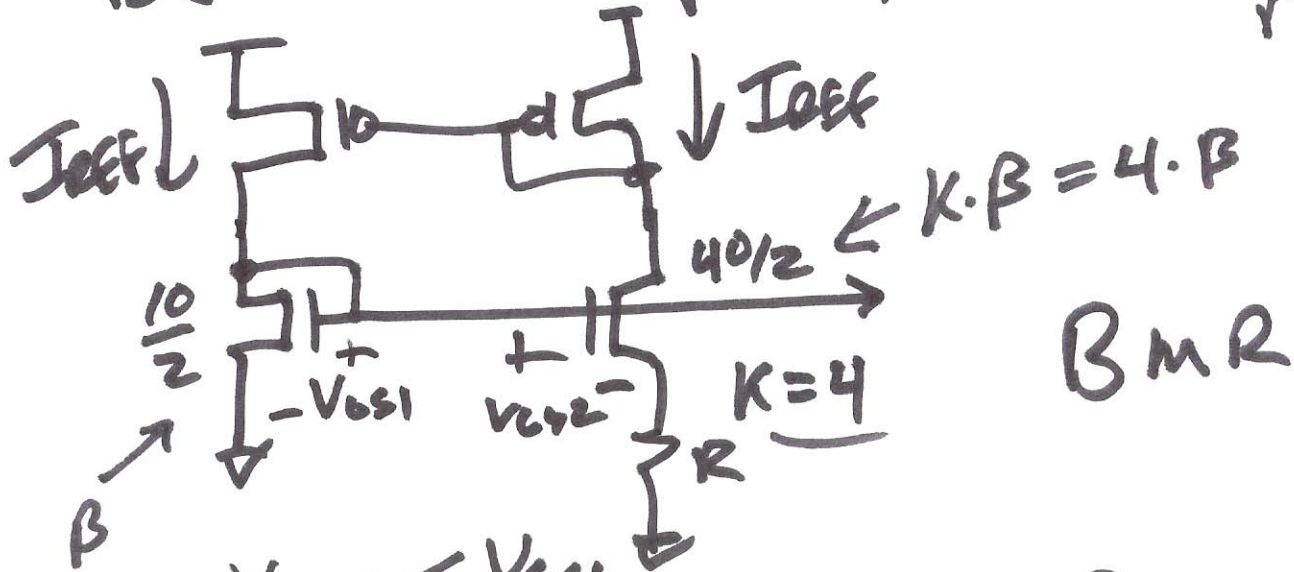
$$I_{REF} \approx \frac{V_{DD}}{R}$$

$$\frac{\delta I_{REF}}{\delta V_{DD}} = \frac{1}{R}$$

$$5 \text{ nA}/\mu\text{V}$$

# Beta - Multiplier, self-biased reference

Start-up  
Ckt  
Not  
Shown



$$V_{GS2} < V_{GS1}$$

$$V_{GS1} = V_{GS2} + I_{REF} \cdot R$$

$$V_{GS} = \sqrt{\frac{2I_D}{\beta}} + V_{THN}$$

$$\sqrt{\frac{2I_{REF}}{\beta}} + V_{THN} = \sqrt{\frac{2I_{REF}}{K \cdot \beta}} + V_{THN} + I_{REF} \cdot R$$

$$I_{REF} \cdot R = \sqrt{\frac{I_{REF} \cdot 2}{\beta}} \left(1 - \frac{1}{\sqrt{k}}\right)$$

$$I_{REF} \cdot R^2 = \frac{2}{K_P \cdot \frac{W_1}{L_1}} \cdot \left(1 - \frac{1}{\sqrt{k}}\right)^2$$

$$I_{REF} = \frac{2}{K_P \cdot \frac{W_1}{L_1} \cdot R^2} \left(1 - \frac{1}{\sqrt{k}}\right)^2$$

independent of VDD!

if  $k=4$

$$I_{REF} = \frac{1}{2 K_P \cdot \frac{W_1}{L_1} \cdot R^2}$$

$$g_m = \sqrt{2 \cdot K_P \cdot \frac{W}{L} \cdot I_{REF}} = \frac{1}{R} \quad (k=4)$$

.8 PA/ $\mu$ V

11)

