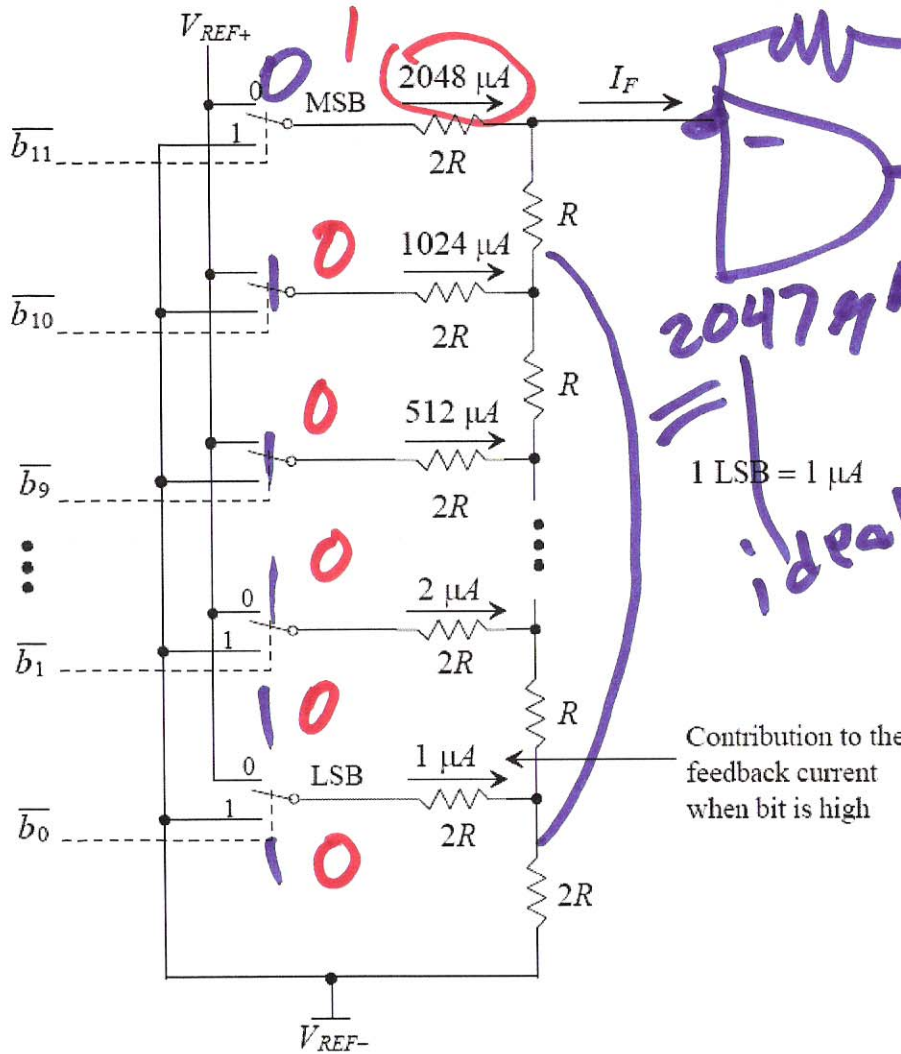


NOV. 8, 2011

Lecture 21



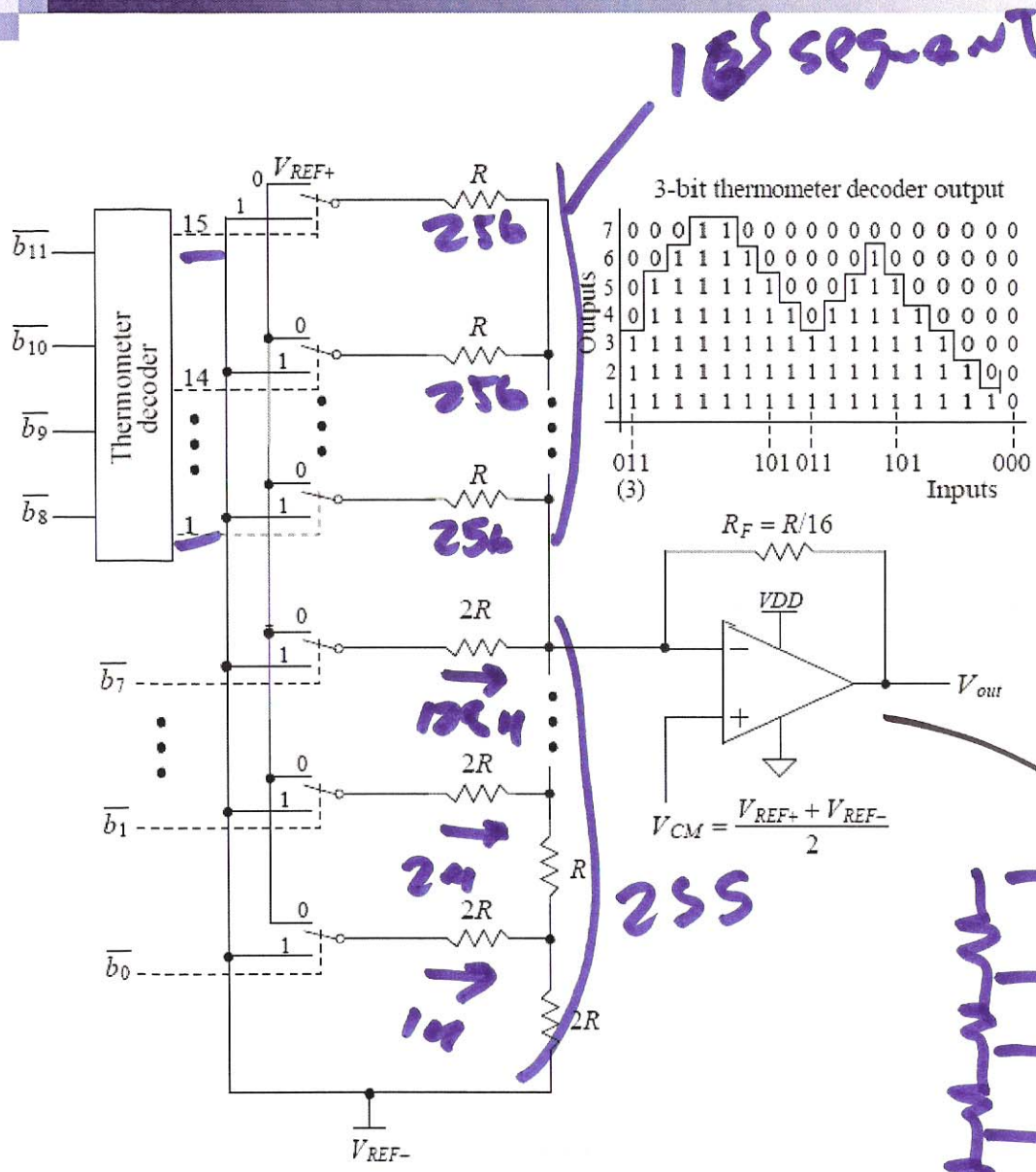
$2048 \mu A \rightarrow 2048 \mu A$   
 $1 \text{ LSB} = 1 \mu A$

$2047 \mu A \rightarrow$   
 ideal

Contribution to the feedback current when bit is high

Figure 30.5 Showing how currents sum into the feedback current.

)



16 segments  
 $4,096 \mu A$   
 $- 256$   


---

 $3840 \mu A$

$2047 \rightarrow 2048$   
 $\frac{14}{2048 \mu A}$

$255 \rightarrow 256$   
 $\frac{14}{255 \mu A}$

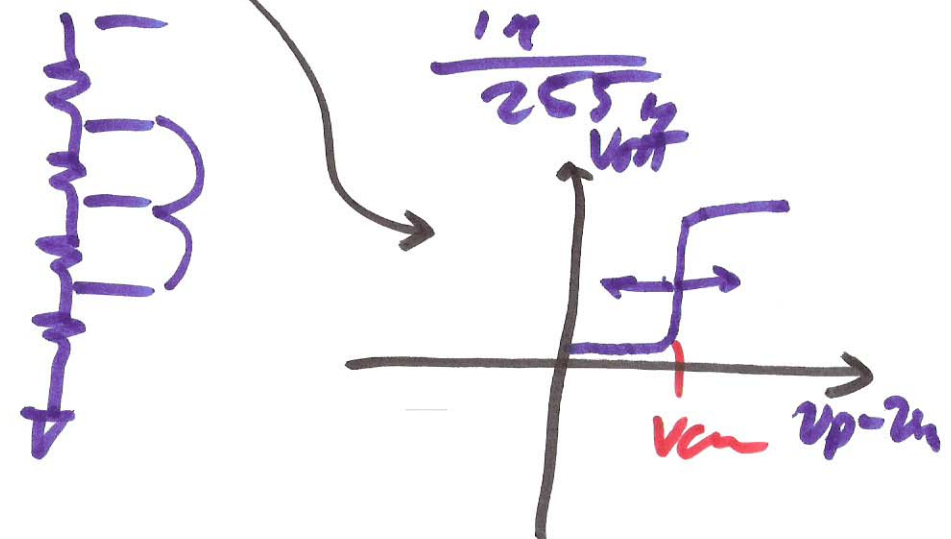
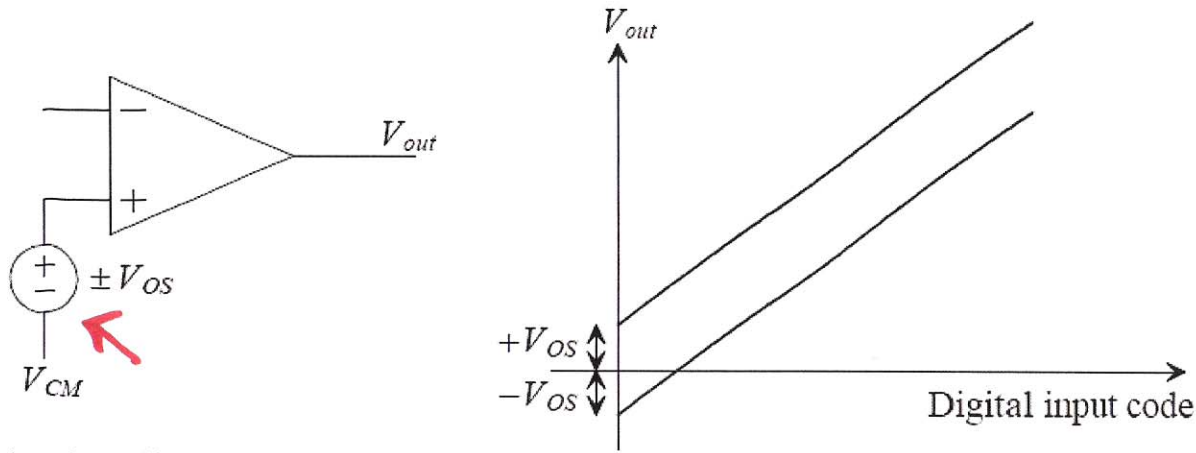


Figure 30.6 Segmentation in a wide-swing R-2R DAC.

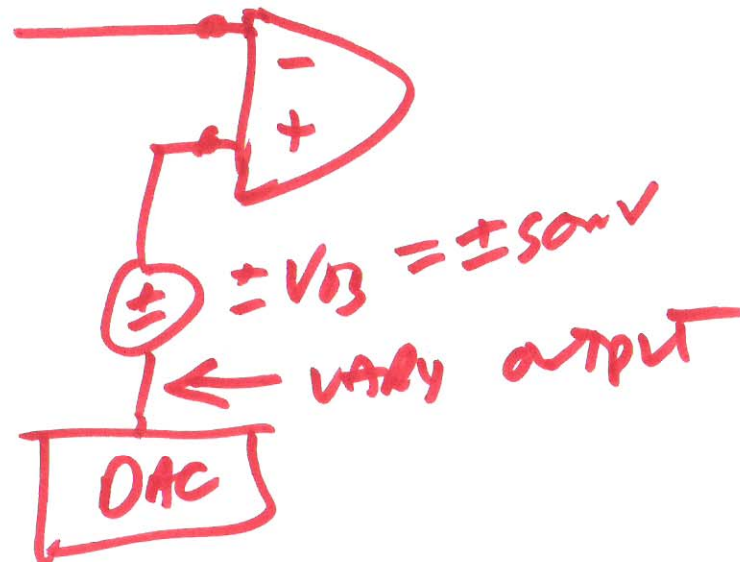
2)



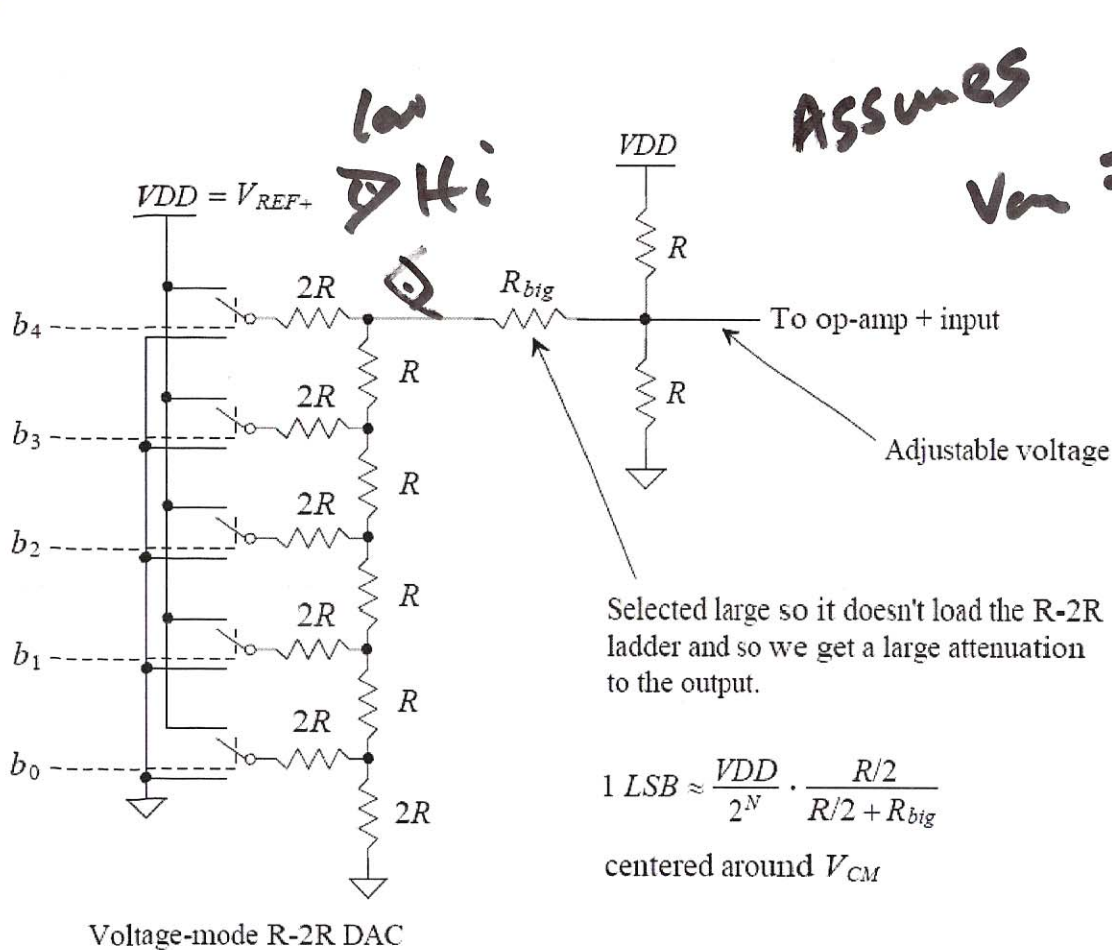
(a) Showing offset voltage in an op-amp.

(b) DAC transfer curves showing offset.

Figure 30.7 Showing how an op-amp offset affects the DAC's transfer curves.



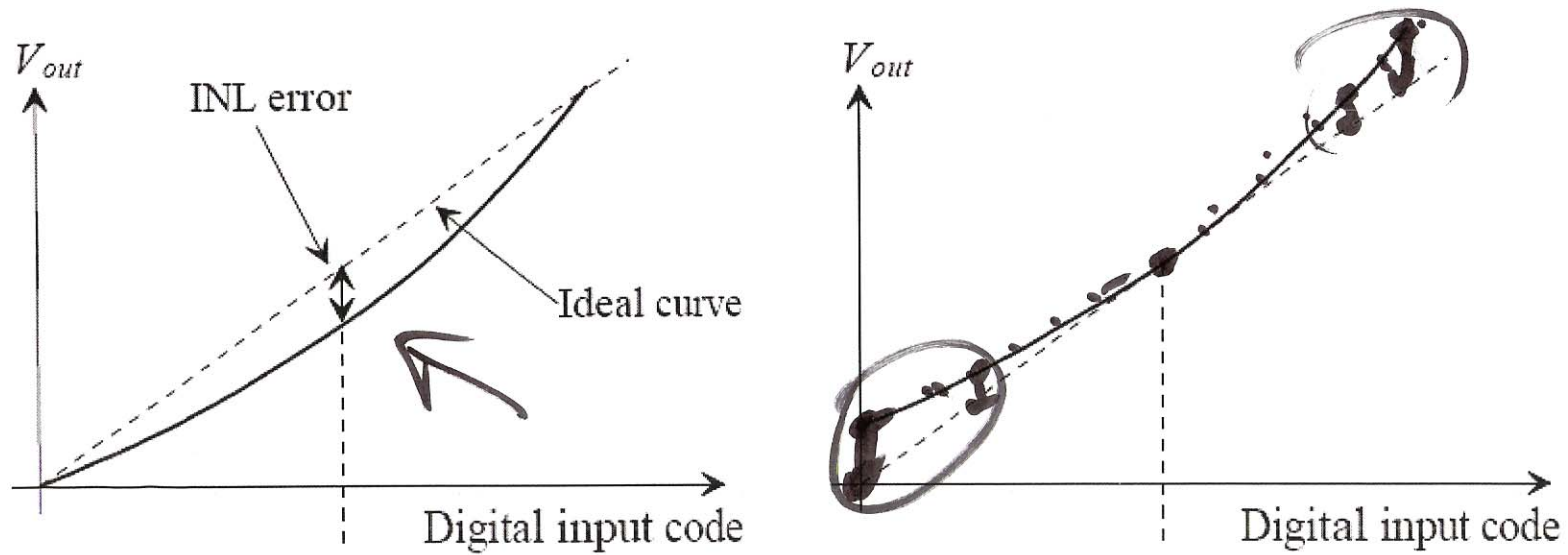
3)



Assumes  $V_{cm} = \frac{V_{DD} - 0}{2}$

Figure 30.8 Trimming circuit for DAC offset.

4)



(a) DAC transfer curves before calibration. (b) DAC transfer curves after offset calibration

**Figure 30.10** Showing how INL can be seen as an offset error.

5)

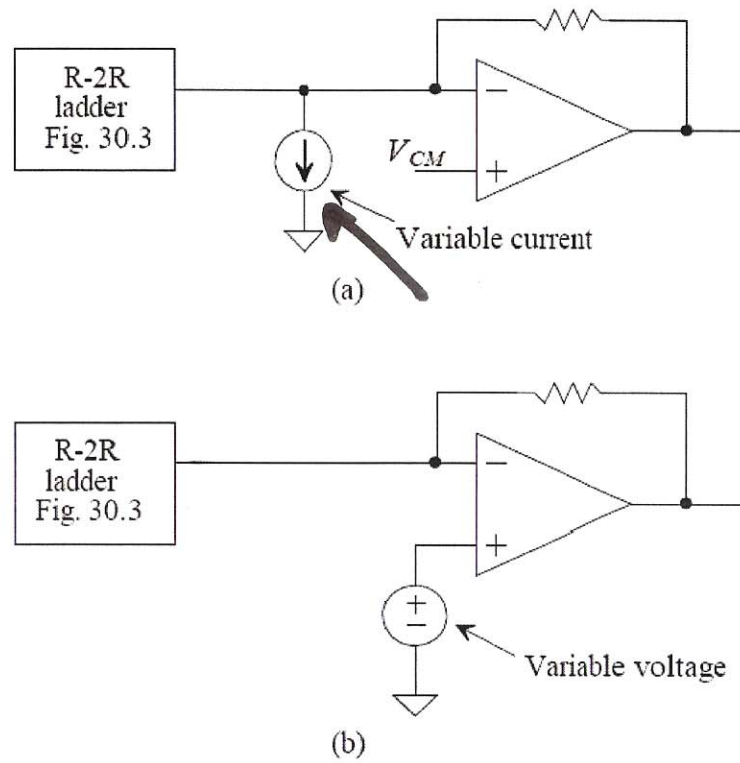
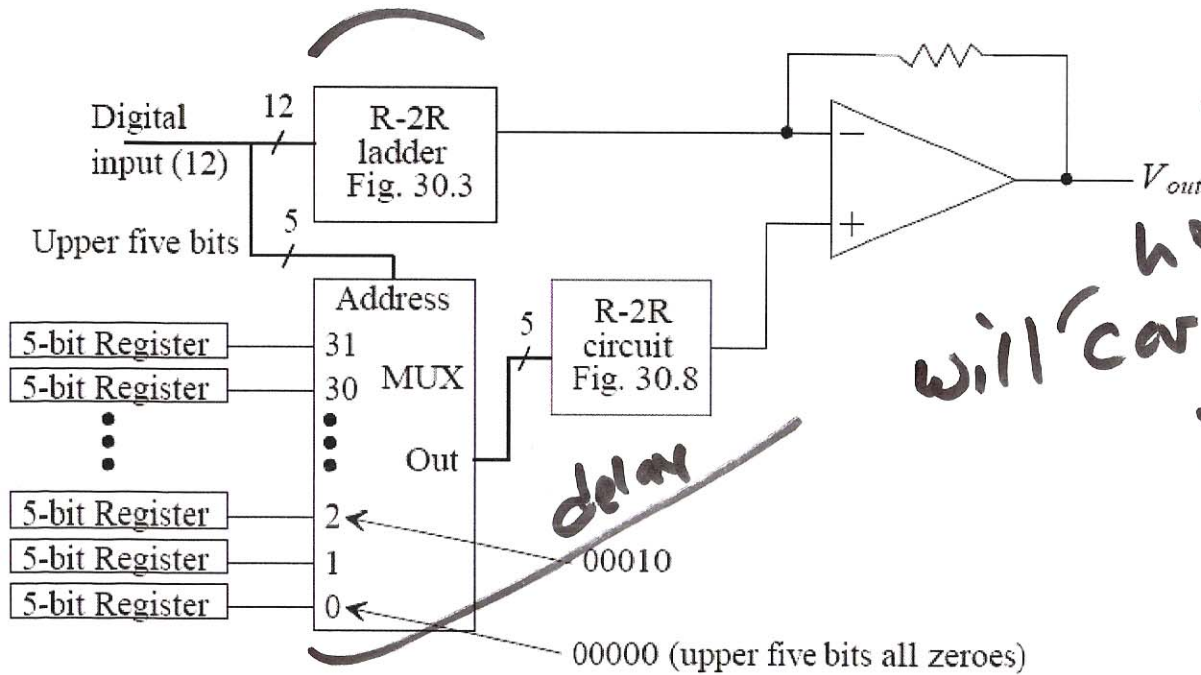


Figure 30.12 Trimming the output of the DAC using (a) current and (b) voltage.

6)



Amplitude width  
Glitch area  
V.S

will correct  
help with  
INL  
offset  
gain

Figure 30.13 Calibration scheme for 12-bit DAC.

0000 0100 0000

64  
0 → 128

128

77

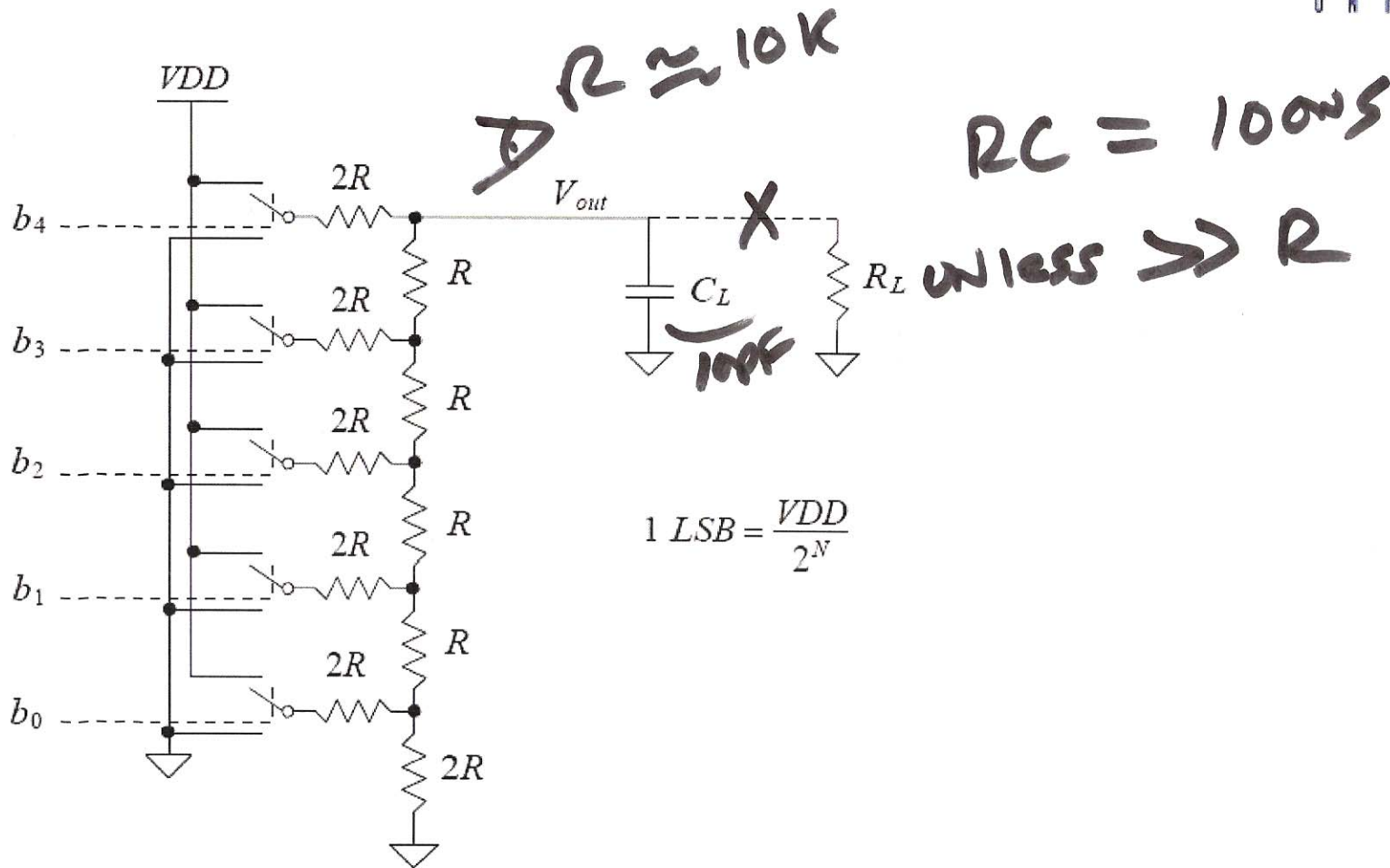


Figure 30.14 Voltage-mode (5-bit) DAC without an op-amp.

8)



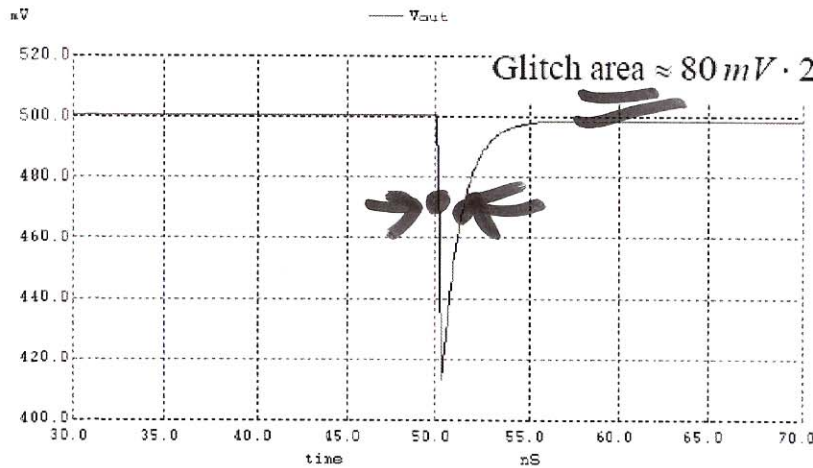
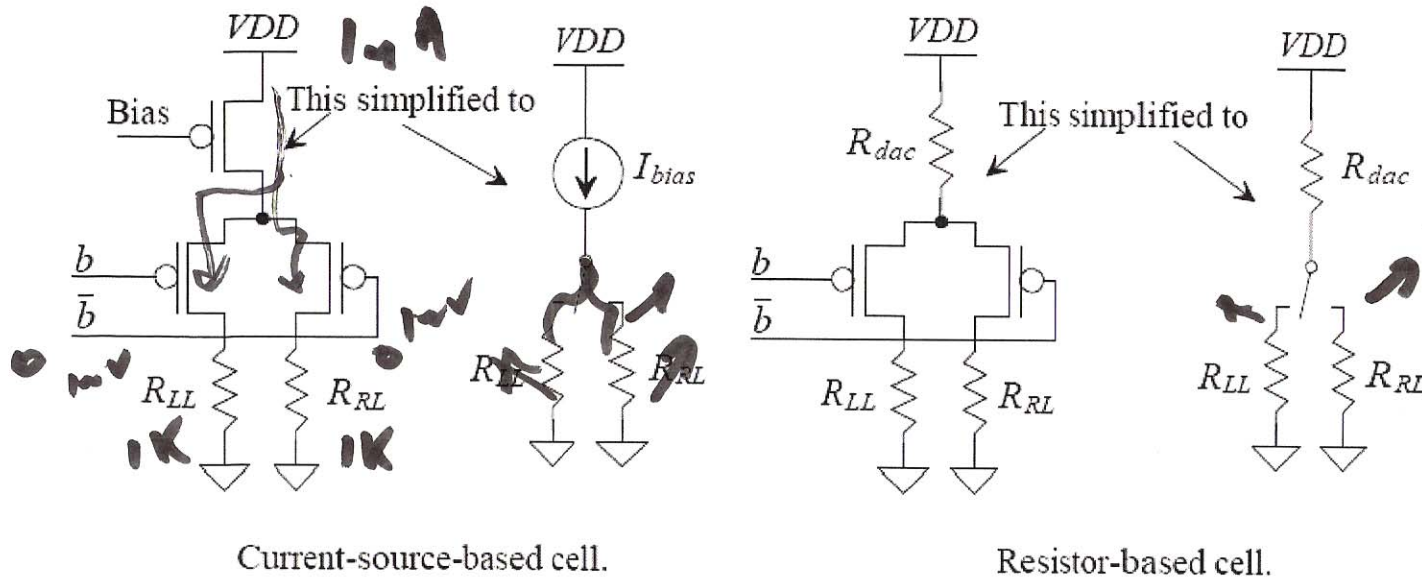


Figure 30.17 Showing glitch if the lower 9-bits are skewed by 200 ps in Ex. 30.2.

don't use  
glitch-energy + -

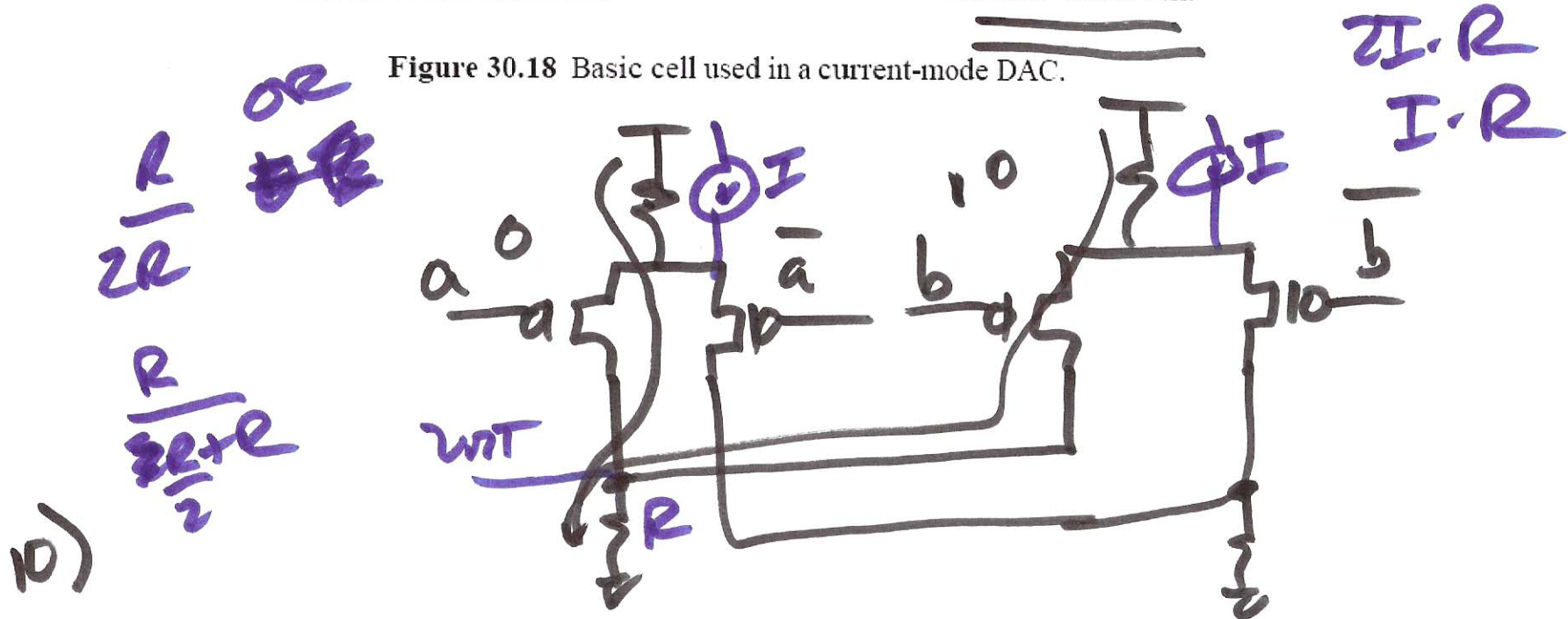
9)

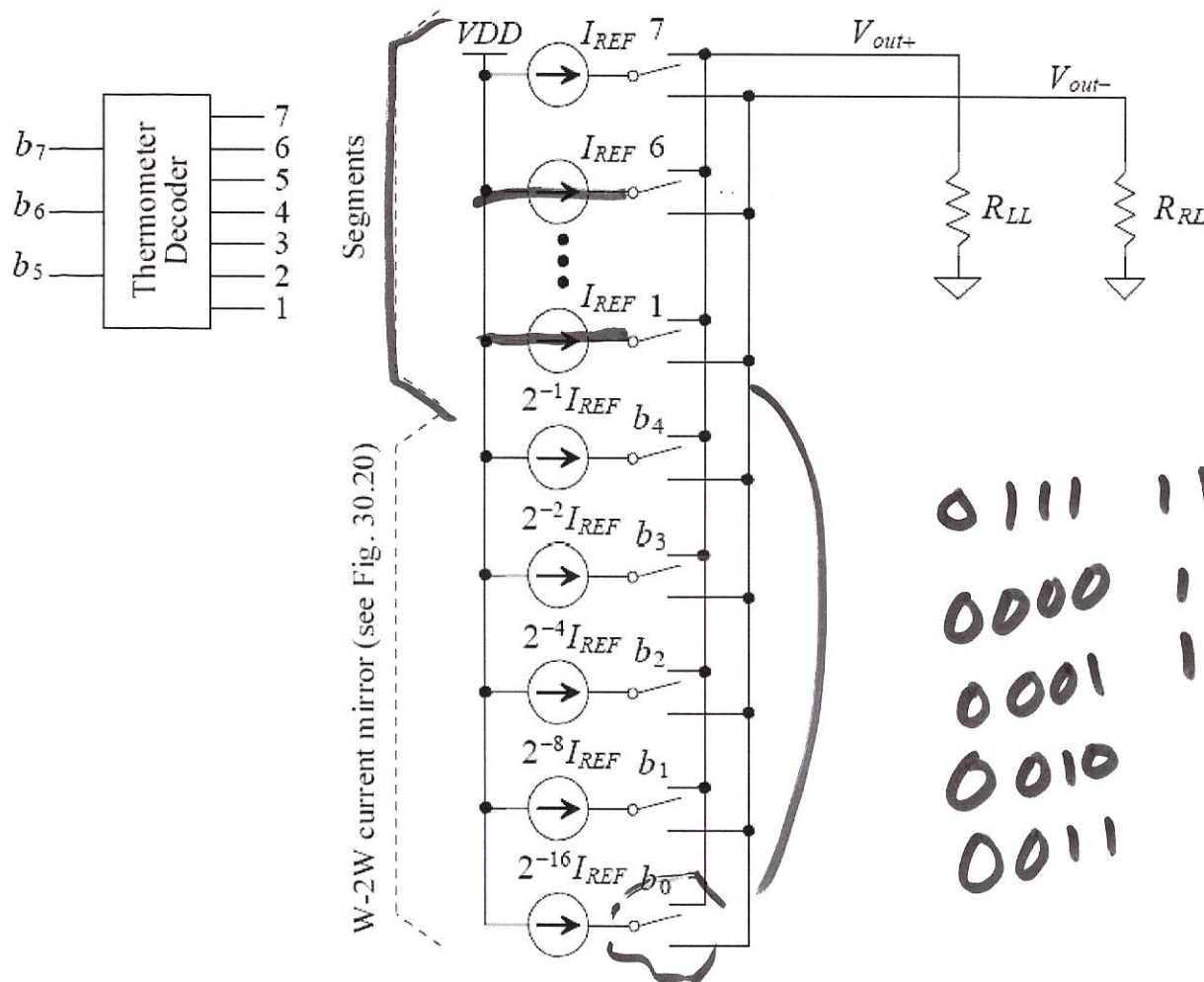


Current-source-based cell.

Resistor-based cell.

Figure 30.18 Basic cell used in a current-mode DAC.





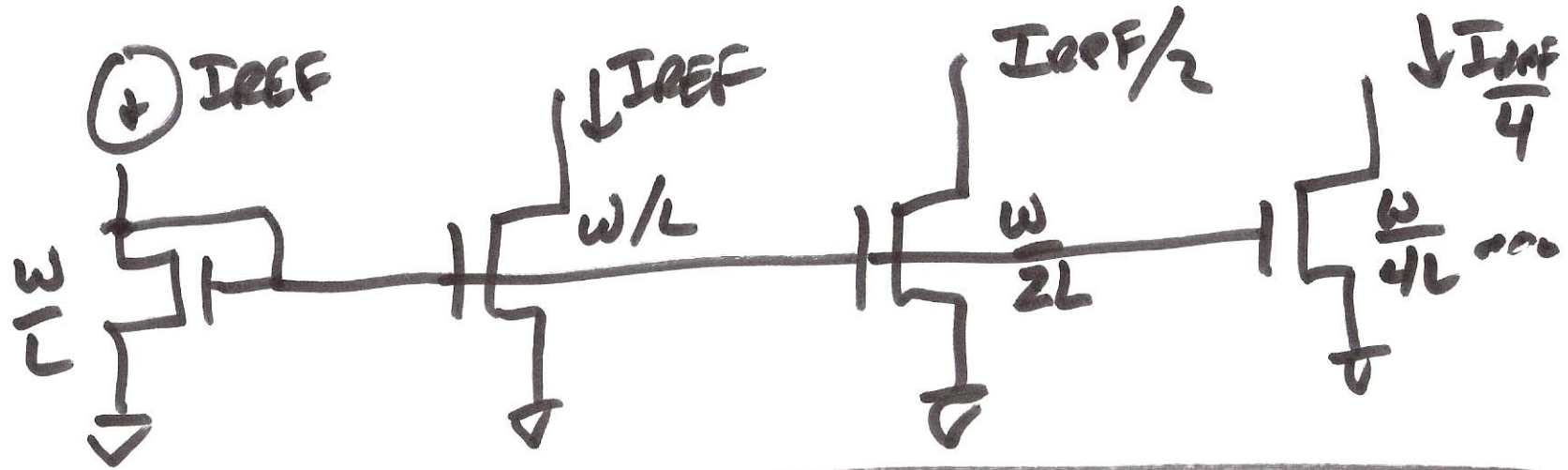
0111 1111  
 0000 1 1 1 1  
 0001 1 1 1 1  
 0010 1 1 1 1  
 0011 1 1 1 1

- NO SEG.  
 - 1 SEG.  
 - 2 SEG.  
 - 3 SEG.

Figure 30.19 Implementation of a current-mode DAC.

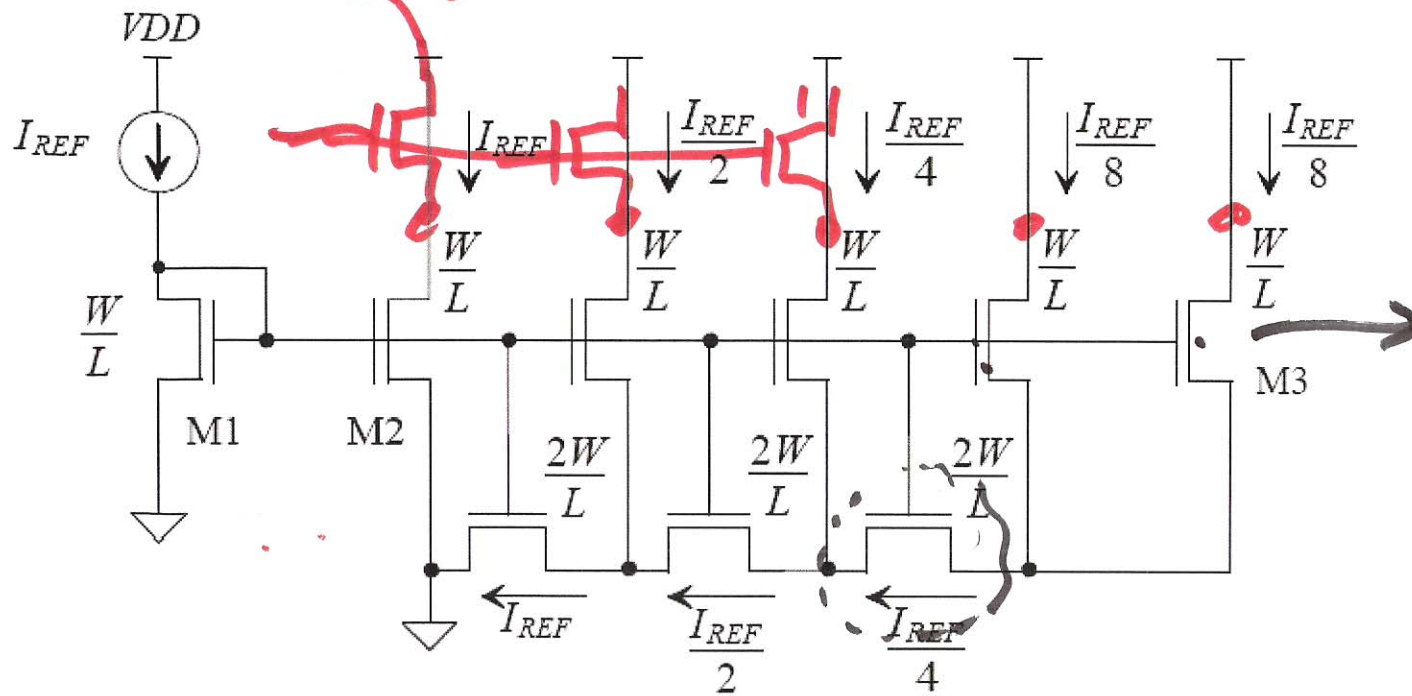
11)

# How NOT to implement binary weighted DACS USING CURRENT SINKS



HAVE TO USE SAME SIZE DEVICE!

to implement the DAC!



$$\begin{matrix} 15 \\ \sqrt{\frac{2W}{L}} \\ 15 \\ \sqrt{\frac{2W}{L}} \end{matrix} = \begin{matrix} 15 \\ \sqrt{\frac{2W}{L}} \\ 31 \end{matrix}$$

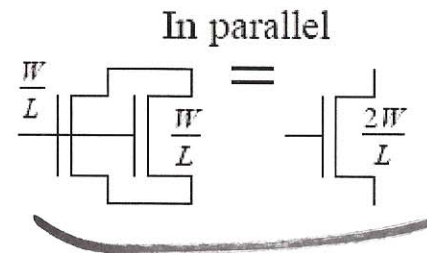
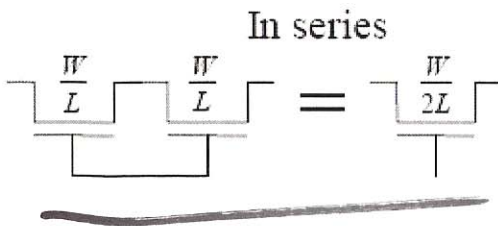
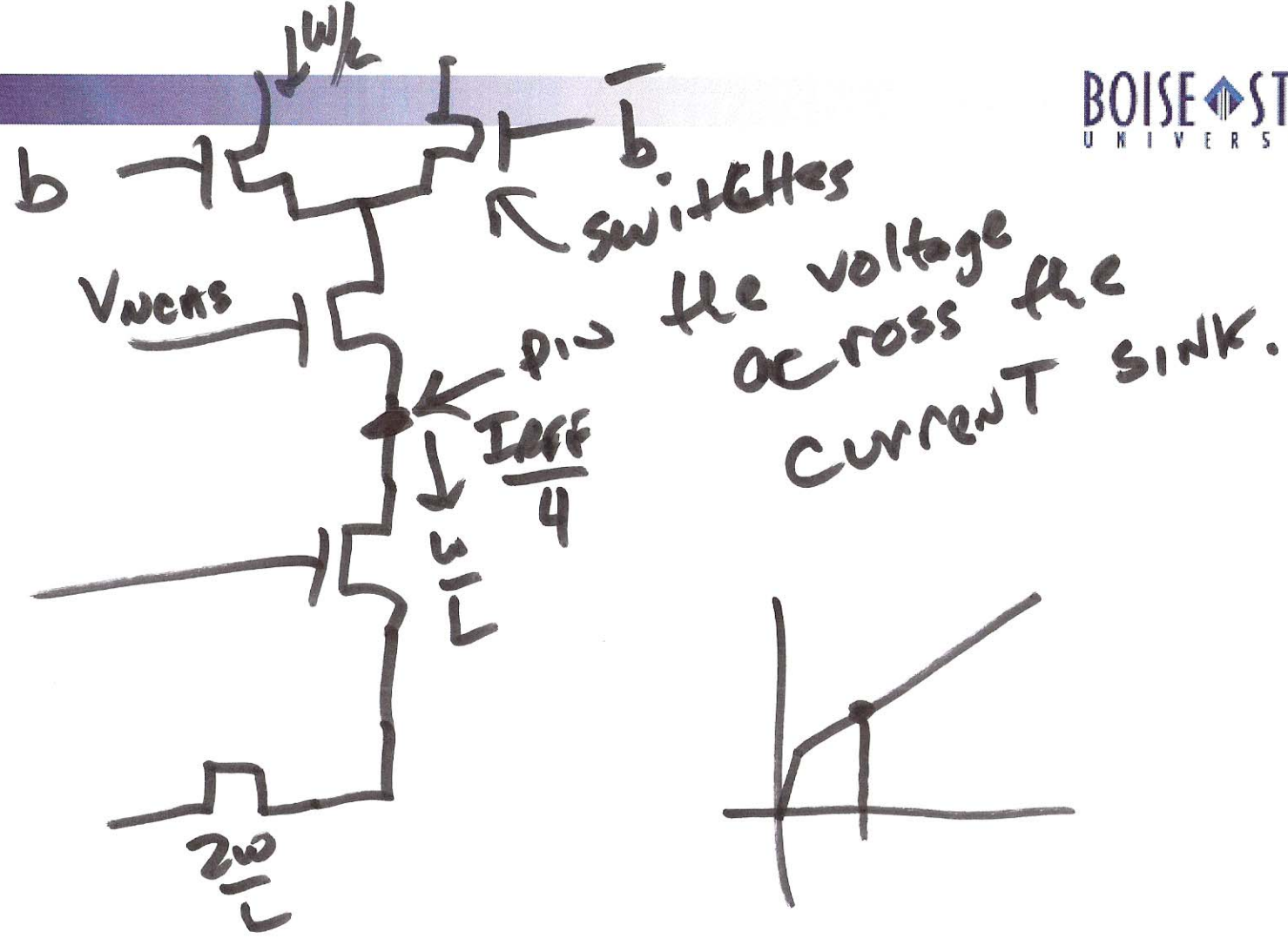


Figure 30.20 W-2W current mirror.

13)



14)

# OP-AMPS IN DATA CONVERTERS



$$V_{OUT} = A_{OC}(V_{IN} - V_f)$$

$$V_f = \frac{V_{OUT} \cdot R_1}{R_1 + R_2}$$

$$V_{OUT} = A_{OC} \left( V_{IN} - \frac{V_{OUT} \cdot R_1}{R_1 + R_2} \right)$$

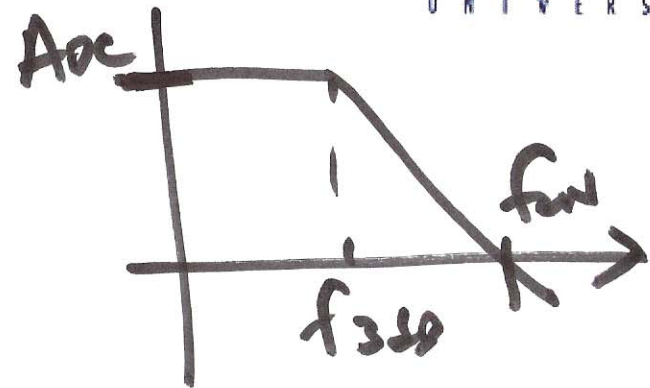
$$\frac{1}{\beta} = \frac{1}{A_{OC} + \beta}$$

$$A_{ideal} - DA = \frac{1}{\frac{1}{A_{OC}} + \beta}$$

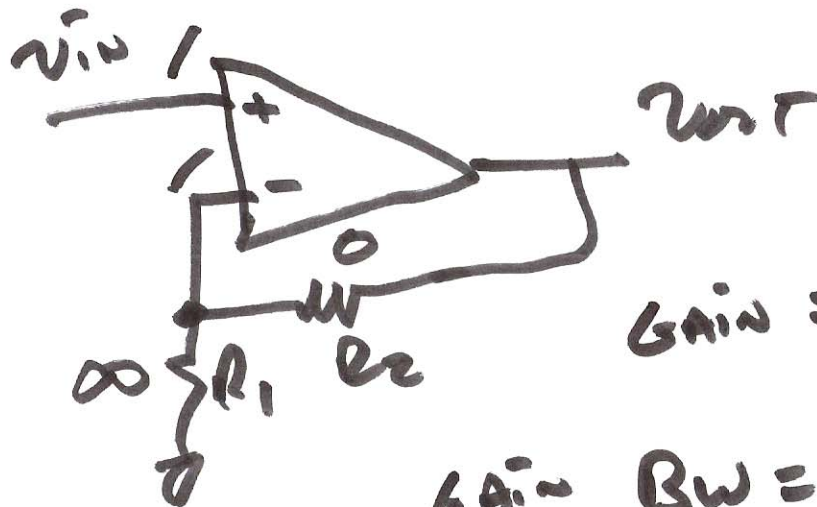
$$V_{OUT} = V_{OUT,ideal} - \frac{1}{2} LSB$$

$$15) \quad \frac{1}{\beta} \left( 1 - \frac{1}{2^{n+1}} \right) \cdot 2^{n+1} \approx \frac{1}{\beta} (2^{n+1} - 1) \approx \frac{2^{n+1}}{\beta} < A_{OC}$$

$$f_{un} \approx A_{oc} \cdot f_{3dB}$$



SERIES - SHUNT



$$GAIN = \frac{1}{\beta} = \frac{R_1 + R_2}{R_1}$$

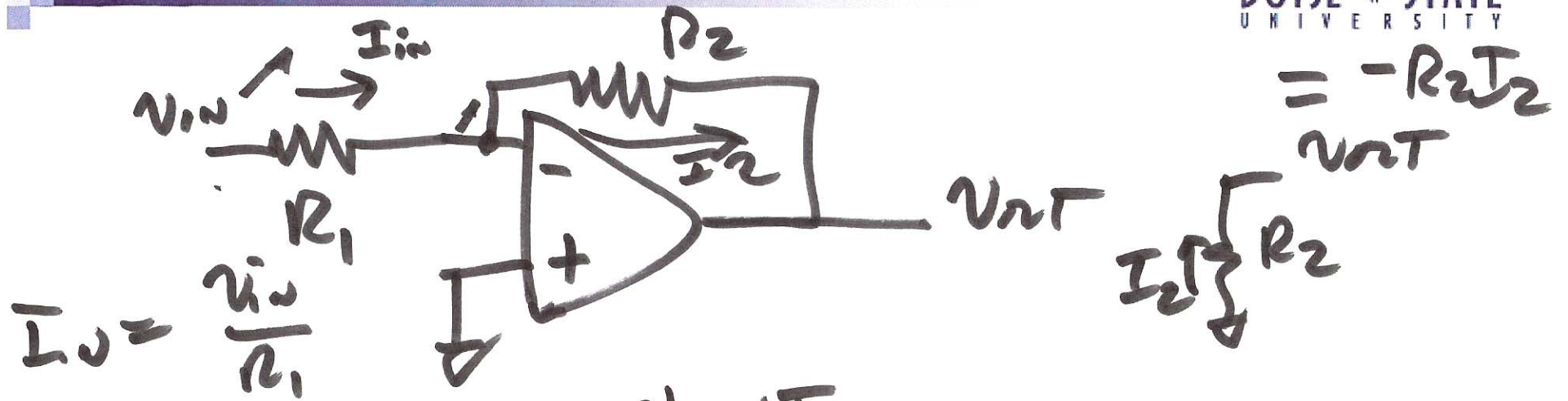
$$GAIN \cdot BW = f_{3dB} \cdot A_{oc} = f_{3dB,CL} \cdot A_{CL}$$

$$BW = \frac{f_{un}}{A_{CL}} = f_{un} \cdot \beta = f_{un} \cdot \frac{R_1}{R_1 + R_2} + 1$$

$GAIN \cdot BW|_{CL} = f_{un}$

(b)





from slide 16 **Shunt-Shunt**  
 $I - V \rightarrow$  transimpedance

$$v_{out} = (0 - v_-) \cdot A_{OL}$$

$$f_{CL} = \frac{R_1}{R_1 + R_2} \cdot f_{un}$$

$$A_{CL} = \frac{v_{out}}{I_{in}} = -R_2$$

Gain  $f_{CL}$

$$= \frac{R_2}{R_1} \cdot \frac{R_1}{R_2 + R_1} \cdot f_{un}$$

17) Shunt-shunt

$$A_{CL} = \left| \frac{v_{out}}{v_{in}} \right| = \left| \frac{-R_2}{R_1} \right|$$

$$f_{CL} \cdot \text{Gain} = \frac{f_{un}}{2}$$

$$G_{AIN} \cdot BW = \frac{R_2}{R_1 + R_2} \cdot f_{wn}$$

inverting

$$G_{AIN} = \left| \frac{R_2}{R_1} \right| \quad BW = \frac{R_1}{R_1 + R_2} \cdot f_{wn}$$



$$-1, R_2 = R_1 \quad BW = \frac{f_{wn}}{2}$$

$$-10, R_2 = 10R_1 \quad BW \approx \frac{f_{wn}}{11} \text{ (inverting)}$$

NON-INVERTING

$$+1, R_2 = 0, R_1 = \infty \quad BW = f_{wn}$$

$$+10, R_2 = 9K, R_1 = 1K \quad BW = \frac{f_{wn}}{10}$$

18)